# NUCLEAR DATA AND MEASUREMENTS SERIES

# ANL/NDM-45

Evaluation of <sup>235</sup>U(n,f) Between 100 keV and 20 MeV

by

W.P. Poenitz

July 1979

ARGONNE NATIONAL LABORATORY, ARGONNE, ILLINOIS 60439, U.S.A.

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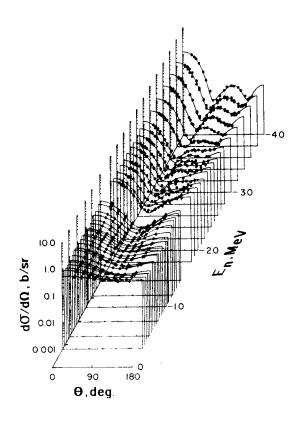
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Applied Physics Division Argonne National Laboratory 9700 South Cass Avenue Argonne, Illinois 60439 USA

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The Nuclear Data and Measurements Series presents results of studies in the field of microscopic nuclear data. The primary objective is the dissemination of information in the comprehensive form required for nuclear technology applications. This Series is devoted to: a) measured microscopic nuclear parameters, b) experimental techniques and facilities employed in measurements, c) the analysis, correlation and interpretation of nuclear data, and d) the evaluation of nuclear data. Contributions to this Series are reviewed to assure technical competence and, unless otherwise stated, the contents can be formally referenced. This Series does not supplant formal journal publication but it does provide the more extensive information required for technological applications (e.g., tabulated numerical data) in a timely manner.

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EVALUATION OF 235U(n.f) BETWEEN 100 KeV and 20 MeV\*

by

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#### ABSTRACT

The <sup>235</sup>U(n,f) cross section was evaluated in the energy range from 100 keV to 20 MeV. Experimental data were included up to the 1978 Harwell Conference on Neutron Physics. The evaluation methodology is discussed in detail. The shape and the normalization of the cross section are evaluated in separate steps. An extensive comparison of the evaluation result with experimental data sets is made.

The shape of the cross section obtained in a preliminary version of the present evaluation and a normalization factor extracted from data provided within the framework of this evaluation were used by the Subcommittee on Standards and Normalizations of the Cross Sections Evaluation Working Group to establish <sup>235</sup>U(n.f) for ENDF/B-V above 100 keV.

<sup>\*</sup>This work supported by the U. S. Department of Energy.

#### I. INTRODUCTION

The requirement for accurate neutron nuclear data is obvious since such data is widely utilized in applications. Hence, many attempts have been made to understand and describe observations made in experiments. This need resulted in a large number of measurements of cross sections directly required in technical applications or used in other measurements, e.g. standards. Theoretical models were developed in order to explain the experimental data, and do predict subsequently nuclide behavior which might be difficult to measure. Evaluated data files were created to supply numerical values needed for applications which represented usable compromises between often contradictory experimental data and theoretical predictions. Earlier evaluations had to use approximations which were more pragmatic than exact as data were sparce in some areas and discrepant in others. However, as experimental data became more abundant and consistent, it was recognized that the general process of arriving at an evaluated data file needed more consideration. Data were often unintentionally correlated due to the use of common mass scales, neutron flux detection techniques or approximations for the interpretation of the experiments. Absolute measurements were made for many nuclei for which relative cross section ratio data were available. This resulted in an overdetermined data system with more measured values than unknown quantities which required a simultaneous evaluation in order to obtain a consistent set of data.

An attempt to evaluate a consistent cross-section-data set for the use in reactor calculations was made in  $1968^2$ , and again with improved techniques in  $1970 \cdot ^1$  Procedures were applied which were similar to those used in the evaluation of thermal cross sections and parameters. An independent but similarly motivated evaluation was also reported in  $1970 \cdot ^4$ . The present evaluation is a first step in a new evaluation of a consistent set of neutron cross sections for the standards ( $^6\text{Li}(n,\alpha)$ ,  $^{10}\text{B}(n,\alpha)$ ,  $^{197}\text{Au}(n,\gamma)$ ) and for other reactions important for technical applications ( $^{235}\text{U}(n,f)$ ,  $^{238}\text{U}(n,\gamma)$ ). The present report discusses the specific evaluation of  $^{235}\text{U}(n,f)$  and describes the general procedures used in the evaluation of specific cross sections and ratios. A later report will contain the evaluation of the other cross sections and the consistency fit. A new simultaneous evaluation seems desirable because the data base has substantially improved since  $1970^5$ , and because improved evaluation procedures have been developed. More recently, a variety of somewhat differently motivated considerations  $^{7-10}$  have been helpful in defining the process described and used in the present evaluation.

#### II. OBJECTIVE EVALUATION PROCEDURES

The knowledge of the magnitude of a quantity comes directly from one or several measurements, or indirectly from a theoretical model, or from established empirical, systematized rules. The theoretical model and the empirical rules depend on other experimental data for the determination of their parameter sets. Therefore, the knowledge one has of a quantity is ultimately the result of experimentation. The measuring process, for various reasons, is subject to uncertainty, thus when the measurements are repeated they will yield different values with different uncertainties. It is the major task of the evaluation process to derive a single "best value"

from the available experimental values and from predicitons from theoretical and empirical models. An objective evaluation procedure is based upon these available data and avoids intuition which might be based upon experience but is probably very subjective in nature.

### 1. Experimental Quantities and the Evaluation Process

The energy dependence of a quantity (cross section, cross section ratio) is usually called its shape. The quantity is known in the total energy range in which the shape is known if the absolute value of the quantity (magnitude) is known at any energy in this range. This corresponds well to the experimental determination of fast neutron reaction cross sections (or ratios). A factor in the determination of the cross section, common to all energies, is the mass of the sample. In many experiments the efficiency for detecting the reaction rate is essentially independent of the neutron energy (e.g., activation cross section experiments) or varies only slightly with energy (e.g., fission cross section experiments). Thus, a major part of the uncertainty and of unknown errors is common to all energies and the cross section can be expressed as

$$\sigma(E) = a \cdot S(E)$$

where "a" lumps together the common factors like mass, efficiency, etc., and S(E) represents the energy dependence (shape). This situation is reflected in the data base. Many of the available data sets were the result of measurements of the energy dependence of the cross section and absolute values were not obtained. In other experiments, absolute values were obtained and measurements were repeated at different energies, thus also providing information about the shape of the cross section. A third group of experiments lead to absolute values but only at one specific energy. All three types of experiments provide valuable information. Experiments which provide only shape information might be able to do so with low systematic uncertainties but the specific setup would result in a large uncertainty of the absolute counting efficiency (and thus the absolute values). Experiments which yield absolute values only at a specific energy may use different techiques which provide values with low systematic, or at least different, uncertainties and different unknown errors but are not applicable over wide energy ranges (e.g., 14 MeV associated particle technique). clear separation of the normalization and the shape in the present evaluation procedure is the result of the de facto separation of a constant factor and its uncertainty and the shape and its uncertainty in the experiments and in the data base.

The importance of the resolution in the interpretation of the reported experimental value is manyfold. The cross section is an average over the flux,  $\phi(E)$ ,

$$\bar{\sigma} = \frac{\int_{0}^{\infty} \sigma(E) \phi(E) dE}{\int_{0}^{\infty} \phi(E) dE}$$

The average energy should be defined as an average over the reaction rate,

$$\bar{E} = \frac{\int_{0}^{\infty} E \sigma(E) \phi(E) dE}{\int_{0}^{\infty} \sigma(E) \phi(E) dE}$$

or the neutron flux,

$$\bar{E} = \frac{\int_{0}^{\infty} E \phi(E) dE}{\int_{0}^{\infty} \phi(E) dE}$$

and derived accordingly, but this is rarely the case. Even if  $\overline{E}$  is derived from the reaction rate,  $\sigma(E)$   $\phi(E)$ , a correction, k, is required to obtain from

$$\sigma(\bar{E}) = k\bar{\sigma}$$

the average cross section at the quoted average energy. The required correction is usually larger if  $\bar{E}$  is derived as an average over the flux only  $(\phi(E))$ . Most frequently the correction was not applied and an uncertainty not accounted for.

The present evaluation is concerned with the evaluation of average (smooth) cross sections. However, fluctuations of the cross sections are known to exist and may influence the interpretation of individual experimental values. The fluctuations would have no impact on the evaluation of the average cross section if the data density were sufficiently high or the resolution poor. A correction factor can be calculated in order to obtain the smooth cross section from the cross section measured with the given resolution if the fluctuations are well enough known (from high resolution measurements). Another approach would be to account for the additional uncertainty.

#### 2. Uncertainties of Experimental Values

Since the object of an evaluation is to provide the best value of a cross section which is derived from experimentally measured values, an uncerstanding and interpretation of experimental cross section values is required. It is assumed that the experimentally measured values have been reported in terms of the following parameters:

- E The average energy at which it was measured,
- ΔE The uncertainty of this energy,
- R The energy resolution or energy spread,
- σ The cross section value,
- Δσ The total uncertainty of the measured value, and
- $\Delta\sigma_{st}$  The statistical uncertainty.

More detailed information may be desirable, however, this appears to exhaust the information extractable from past experiments.

It is in the nature of the measuring process to be uncertain. The true experimental uncertainty is composed of several factors  $^{1,7,13}$  and may be subdivided as follows:

- $\Delta\sigma_R$  The reference uncertainty (mass, reference cross sections, etc.),
- $\Delta\sigma_s$  The systematic uncertainty (estimated or calculated from the uncertainties of models and parameters used to calculate corrections, background subtraction, etc.),
- $\Delta\sigma_{\text{st}}$  The statistical uncertainty (caused by the limited number of events counted),
- Δσ<sub>a</sub> The accidental error, which may be revealed if the identical experimental is repeated (i.e. reproducibility),

 $\Delta\sigma_{\mathbf{u}}$  The unknown error, which is systematic in nature and caused by not recognizing necessary corrections or underestimating uncertainties.

Δσ<sub>ps</sub> The psychological error which is caused by satisfaction with agreement obtained with values reported by others, thus neglecting the search for additional effects in the measuring process or equipment which would require corrections, or, the opposite, that is the dissatisfaction with a disagreement with prior reported values and the subsequent search for onedirectional corrections,

 $\Delta\sigma_{pe}$  The personal error which is associated with the specific experimentor (Bessels observation of differences of experimental results obtained by leading astronomers of his time is noted in Ref. 13).

The reference uncertainty is usually beyond the responsibility of the experimentor. Sometimes it is possible to trace errors and improvements can be made on the reported measured value. The systematic uncertainty is the major responsibility of the experimenter. The statistical uncertainty is the best defined uncertainty and usually the only one the mathematical faculty bothers to deal with. Accidental errors could be limited to at best the statistical uncertainty by frequently repeating the experiment. However, experiments which involve long measuring times are not easily repeated. Some values can be recognized to have an accidental error, e.g., if the shape was measured and a singular point falls outside a range given by the statistics and known fluctuations of the cross section.

Quoting the existence of personal errors and psychological errors separated from the unknown error is of interest to gain some understanding of possible causes for unknown errors. In effect they affect the evaluation in a similar way as the unknown error though the psychological error might produce, as a side effect, historical trends in reported cross sections as shown in Ref. 1.

The quoted uncertainty,  $\Delta \sigma$ , is usually the square root of the sum of the squares of the reference uncertainty, the estimated or calculated systematic uncertainty of the experiment, the statistical uncertainty and sometimes the reproducibility (accidental error), i.e.

$$\Delta\sigma^2 = \Delta\sigma_r^2 + \Delta\sigma_s^2 + \Delta\sigma_{st}^2 \ (+ \Delta\sigma_a^2) \quad .$$

Whereas most experimenters now quote the uncertainty of their measurement this way, some quote only a partial uncertainty, for example, the statistical uncertainty and the systematic uncertainty, and thus give the impression of a higher accuracy of the measured quantity than actually achieved. The evaluator must take care to add the normalization uncertainty in order to weight different data on an equal basis.

The energy uncertainty,  $\Delta E,$  and the resolution, R, result in cross section equivalent errors and uncertainties. The energy uncertainty may be subdivided in a similar way as the cross section uncertainty. One can translate  $\Delta E$  into an additional cross section uncertainty,  $\Delta \sigma_E,$  by approximating

$$\Delta \sigma_{E}^{2} = \frac{d\sigma}{dE}^{2} \Delta E 2 + \frac{d\sigma}{d\sigma_{R}}^{2} \frac{d\sigma_{R}^{2}}{dE}^{2} \Delta E^{2} + \sum_{i}^{d\sigma} \frac{d\sigma_{G}^{2}}{dE}^{2} \frac{dF_{i}^{2}}{dE}^{2}$$

(linear regression), where the first term is the cross section uncertainty caused by the energy dependence of the measured quantity, the second term is that caused by the reference cross section and therfore does not apply to experiments which use absolute techniques or counters because they do not depend (in first order) on other cross sections. The last term accounts for the energy dependence of efficiencies and corrections which are part of deriving the quoted cross section. Often, the last term is small compared with the first two as a reuslt of the second order nature of corrections and the choice of flat-efficiency detectors. The second term is an important contribution which may reach or, in the case of the  $\mathrm{H}(n,n)$  cross section, exceed the uncertainty of the reference cross sections itself which is accountable as  $\Delta\sigma_R$ .

## 3. The Handling of Discrepant Data Sets

Data are usually considered discrepant if they differ by more than their quoted uncertainties. An unknown error causes, with high probability, such discrepancy if it exceeds two or three standard deviations. The unknown error may be found in further analysis of the experiment by the experimenter or by others. If such is the case, a correction can be applied and the corrected value used in the evaluation. The values, thus entered, will still have unknown errors. If the number of independent data sets is sufficiently large, it is believed that an appropriate averaging will provide a better knowledge of the cross section and unknown errors might be assumed in individual experiments which disagree with the average outside the total estimated uncertainty of the experiment. However, it must be relaized that the quoted total estimated uncertainty represents in most cases only a probability distribution and a criteria must be established for suggesting an unknown error and adding to the uncertainty. In the present evaluation a 2 (2 standard deviations) criteria is used to double the given estimated uncertainty. Based upon the assumed normal distribution, this means that the probability for the quoted uncertainty of the experimental value to describe the real error of the vlaue is less than 2.3%.

Often data discrepancies are not a problem of one or two sets (which are assumed to be solvable with the  $2\sigma$  criteria) but exist between several data sets on the one hand and several others on the other hand. The data are reanalyzed in such cases, searching for specific resolutions of the

Corrections are applied and the data are re-entered into the evaluation if such solutions can be found. The resolution of the discrepancies by additional experimental work is recommended if solutions cannot be found by reanalysis. The discrepant data remain part of the data base until the ultimate resolution of such discrepancies. The evaluated result will be an average of the discrepant data and the error files will indicate the dispersion of the data. Such a procedure specifically avoids the assumption that only one of the two data sets is correct which would amount to taking a less than 50-50 chance of being totally right or totally wrong. The average of the discrepant data is at the largest probability for the true values, however, the implication of the existence of unknown errors is that the suggested solution may be half wrong or only half right. The acceptance of the average of discrepant data as part of the present evaluation procedure should reduce the cascading damage caused by a 50% probable totally wrong solution by one half.

# III. THE EVALUATION OF 235U(n,f) CROSS SECTION DATA

The present evaluation is an evaluation of the energy-averaged 235U(n,f) cross section. It does describe gross structure (e.g. the step at 1 MeV, the bump at 2 MeV, the rise due to 2nd and 3rd chance fission). It does not describe "fine structure fluctuations" which are known to exist even above 0.1 MeV and it does not describe detailed features of some of the gross structure which might exist. However, such details of the structure are considered and included in the correction and interpretation of individual data points which are used in the evaluation of the average cross section.

# 1. The Present <sup>235</sup>U(n,f) Data File

The present data file consists of all data reported up to and including the Conference on "Neutron Physics and Nuclear Data for Reactor and Other Applied Purposes" which took place at Harwell in September 1978. Data reported earlier than the publication by White 14 were only included if reevaluations were available. It is assumed that older data would need substantial reevaluation efforts because data for neutron source reactions, cross sections and other critical values which might affect the results have undergone substantial changes. Moreover, the weight of these data would be very small as they were usually reported with uncertainties in the 5-10% range. Thus, the effort and costs of a major reevaluation of these older data seemed not to be justified. It should be noted, however, that older data are usually higher than the presently evaluated data and their inclusion would raise the present result. Some of the more prominent older data sets, though not included in the evaluation, are compared with the present result in Section IV.

The major part of the present data file is that documented in Ref. 15 but the file was updated to include newer data. The format of this file is standardized and is such that it permits its ready use in evaluations. Data measured relative to the hydrogen scattering cross section were updated to  $ENDF/B-V^{16}$  values (Hopkins-Breit analysis  $^{17}$ ). Instead of using actual ENDF/B-V tabulated values it was found more convenient to use the expression

$$\sigma_{\text{H}} = 2.786 \cdot [1 + 0.2412 \cdot \text{E} + 0.0029 \cdot \text{E}^2]^{-1} + 17.68 \cdot [1 + 7.5644 \cdot \text{E} + 0.1534 \cdot \text{E}^2]^{-1}$$

which, up to 20 MeV, seems to describe ENDF/B-V within 0.15% or better.

A quantity of importance for the normalization of shape data which extend to the eV-energy range is the 7.8-11.0 eV fission cross section integral. Table I lists values which were referenced to the present thermal cross section of ENDF/B-V (583.5b). These values result in a weighted average of 243.1 ± 1.3 b-eV. One of the values measured by Gwin appears to be outside two standard deviations set as a limit in Section II.3. Doubling the uncertainty of this value results in an weighted average of 243.7 ± 1.0 b-eV. A more recent value measured by Wagemans<sup>25</sup> is  $\overline{244.3}$  b-eV and a preliminary value by Brown<sup>26</sup> is  $247.2 \pm$ 4.9 b-eV. A fit of thermal parameters 43 resulted in a 0.8% higher thermal neutron fission cross section for <sup>235</sup>U which would increase the integral considered here. Recent findings<sup>27</sup> indicate that measurements using BF3 counters may have resulted in low values, thus the weighted average would increase further. Until clarification of this latter effect and finalization of the data by Wagemans and by Brown, the value 243.7 ± 1.0 b-eV will be used for normalization.

Fluctuations in the 235U(n,f) cross sections are well established below 100 keV and several data sets also indicate fluctuations in the cross section above 100 keV. Figure 1 compares data by Gayther<sup>27</sup> and Wasson.<sup>28</sup> A smooth cross section was subtracted in order to permit an easier comparison of the data. Though there seems to be agreement at some energies, there is disagreement at many others. Most dips in the data by Wasson<sup>28</sup> appear to be correlated with resonances in iron. A data set by Gwin<sup>20</sup> has some gross structure not seen in the other data sets. Because of these inconsistencies, corrections were not applied to any data. The analysis of cross section uncertainties caused by fluctuations as a function of the resolution of the experiment by Bowman<sup>30</sup> was used to estimate the additional uncertainties. Fluctuations of the cross section at higher energies were reported by Albert31 but could not be verified. 32,33 More recently, measurements by Osterhage et al. 34 show large fluctuations, but it appears that these data suffer from substantial statistical uncertainties and energy scale problems.

The data sets used in the present evaluation are given in Appendix I. Renormalizations due to changes of the reference cross section, fission integral and fission masses were applied to the data sets resulting in permanent changes. Additional uncertainties due to energy uncertainties and cross section fluctuations were taken care of during the different stages of the evaluation.

TABLE I. The Fission Integral from 7.8 to 11.0 eV

Author	Reference	Value/B-eV	
Deruytter, Wagemans	18 <sup>a</sup>	243.07 ± 2.4	
Czirr	19	243.9 ± 1.9	
Gwin	20 <sup>a</sup>	235.92 ± 3.5	
Gwin	21	245 ± 3	
ORNL/RPI	22 <sup>a</sup>	241.3 ± 4.8	
Bowman	23 <sup>a</sup>	251.91 ± 7.6	

aValues updated as quoted in Ref. 24.

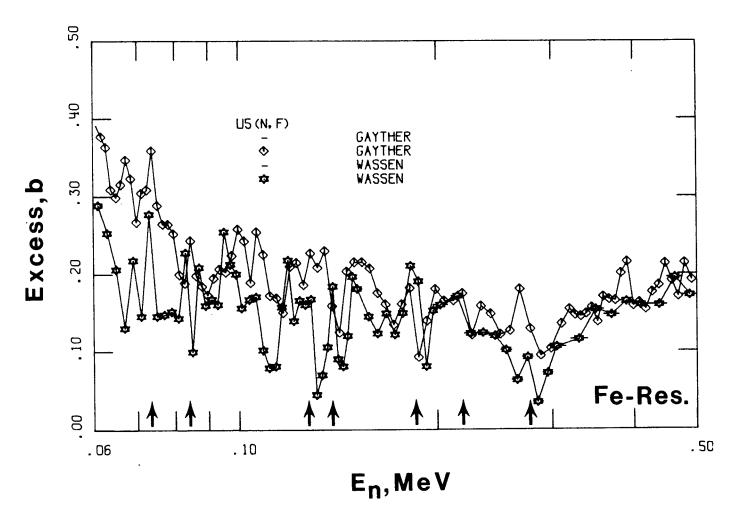


Fig. 1. Comparison of the Structure Obtained by Wasson<sup>28</sup> and Gayther<sup>27</sup> in the Energy Range from 60 keV to 500 keV. A smooth "background" cross section was subtracted in order to better facilitate comparison.

TABLE II. Shape Evaluation Input

Set	Set Name	Energy Range MeV
1 2 33 4 51 and 52 6 71 72 8 10 111 and 112 17 153	Smith <sup>29</sup> Barton <sup>40</sup> Czirr <sup>38</sup> , Combined Set Kari <sup>39</sup> Szabo <sup>44</sup> White <sup>14</sup> Poenitz I <sup>41</sup> , <sup>42</sup> Poenitz II <sup>42</sup> Gayther <sup>29</sup> Wasson <sup>28</sup> Kaeppeler <sup>37</sup> Wasson and Meier <sup>45</sup> Carlson, Combined Set U. Michigan	2.2 - 20.5 1.0 - 6.0 0.75 - 20.0 1.0 - 20.0 0.01 - 5.5 0.04 - 14.1 0.2 - 8.2 0.03 - 3.5 0.001 - 0.95 0.005 - 0.75 0.4 - 1.0 0.25 - 1.2 1.2 - 0.2 0.14 - 0.96

#### 2. The Evaluation of the Cross Section Shape

Table II indicates the data sets which were used in the calculation of the presently evaluated shape. Data were not modified beyond the permanent modifications indicated in the file and the modifications to the uncertainties discussed below. An energy grid with 63 values was established for use in the shape evaluation. This grid was found sufficient to describe all gross structure of the average cross section between 0.1 and 20.0 MeV. Experimental data points were extrapolated to the grid energy,  $E_i$ , if they were found in the interval  $[E_i - 0.5 \ (E_i - E_{i-1}); E_i + 0.5 \ (E_{i+1} - E_i)]$  using the shape of the cross section in the range  $[E_{i-1}, E_{i+1}]$ . This shape was obtained from another evaluation.

Interpolation was attempted by a power curve, a 2nd-order polynomial, and a linear curve. Finally, a power curve was used below 1 MeV and linear interpolation above. Little difference for any choice of curves of interpolation can be expected for a sufficiently small grid and reasonably random (in E) distributed data points. The choice of the cross section used in this extrapolation procedure does not influence significantly the outcome of the shape evaluation.

The uncertainty of the value at a grid point was determined from a variety of components. The total uncertainty of the experimental points was increased by the uncertainties caused by the uncertainty in energy (see Sect. II.2) and the uncertainty due to cross section fluctuations. The former requires that the energy uncertainty be known, the latter requires that the resolution be known. For experiments which did not quote the energy uncertainty it was assumed to be 20% of the resolution for Van de Graaff type experiments and 10% of the resolution for Linac type experiments. The resolution was assumed to be 1% of the energy for Linac type experiments and 5% for Van de Graaff type experiments if it was not given. The uncertainty of the grid point was reduced by part of the statistical uncertainty if several experimental data points contributed For this purpose it was assumed that the statistical uncertainty originated from a limited number of events detected in the experiment. The uncertainty of the grid point is reduced by the normalization uncertainty which applies only to absolute measurements. An additional uncertainty of the grid point is that caused by the procedure in obtaining it. which was estimated to be 0.5%.

The values obtained from one data set provide cross section ratios between any two of the energy grid points for which they are available. In forming the ratios,  $R_{ik}$ , between the cross section values,  $\sigma_i$ ,  $\sigma_k$  from these grid points the arbitrary or absolute normalization of the data set is removed. The different experiments provide contributions to some of the  $R_{ik}$ 's which yield a weighted average  $\overline{R}_{ik}$  with an uncertainty  $\Delta R_{ik}$ . By summing (weighted) the contributions to any  $\sigma_i$ , one obtains a system of equations which can be resolved in a "roll-back" procedure by defining a starting point  $\sigma_1$  = x, where x is arbitrary. The roll-back may as well be started on the high energy side, that is, with setting  $R_{63}$  = y, where y again is arbitrary. Results starting from different sides will be expected

to differ somewhat, reflecting data uncertainties and inconsistencies. Figure 2 shows the results obtained from the shape evaluation with the techniques described above. At this stage an eyeguide curve was drawn through the calculated values which represents the expected physical behavior of the cross section better. The paper by Moore gave guidance over most of the energy range. The origin of the step at 1 MeV is well understood however, its detailed structure is unknown and difficult to extract from the available data. In this range the largest difference occurs between the two calculated shape data sets, it is due to the weight of Czirr's shape data which suggest a much larger step than all other data sets. The fourth chance fission threshold did not show up in the calculated values because of the contradictory results of the data by Kari and by Czirr above 18 MeV and was introduced at this stage.

## 3. Evaluation of the Normalization

The weighted average of factors obtained from the different absolute data sets was used for the normalization of the arbitrarily normalized shape curve. These factors are given in Table III and were derived as the weighted average of the ratios of the data and the values of the shape curve. The total uncertainties were used to determine the weights. The cross section uncertainties caused by energy uncertainties and cross section fluctuations The uncertainty of the shape curve was also taken into account. The uncertainty of the normalization factor was determined as the average of the uncertainties for the individual ratios and reduced by part of the statistical uncertainty if more than one value contributed. Table III shows in one column all normalization factors and in another column a selection of such In the latter, the three Russian sets (16, 12, 14) were excluded because these data are not well documented and do not permit a detailed analysis. the measurement by Alrasov may be superceded by the work by Arlt. An "Information-Publication" by the Technical University of Dresden shows Alrasov as a coauthor for the measurement reported by Arlt et al. The shape of the data by Barton et al. 40 shows several features which cannot be seen in any other data set (for example, a very flat shape between 1 and 2 MeV, a "step-up" around 3 MeV). Therefore, only the 3 MeV value was used from this data set to determine the normalization factor. The value at 3 MeV is the result of many consistency-check measurements described by Barton et al. 40 The BND data published in 1976 by Poenitz<sup>41</sup> were used in the selected set because the BND data<sup>42</sup> from 1974 are not totally independent from the VSO<sub>4</sub>bath measurement. The data by Kaeppeler were excluded from the column of selected values because the shape appears not to agree with any other measured shape. Finally, the Cf-source average value from the University of Michigan was excluded because it is not independent from the photo-neutron source measurements by the University of Michigan and the neutron source strength value used by Heaton et al.

The weighted and the unweighted average of the normalization factors agree very well, showing that no bias was introduced by data with lower uncertainties. The average from the column of selected values given in Table III is used in the present evaluation for the normalization of the shape curve. Table IV shows the average differences of the absolute data

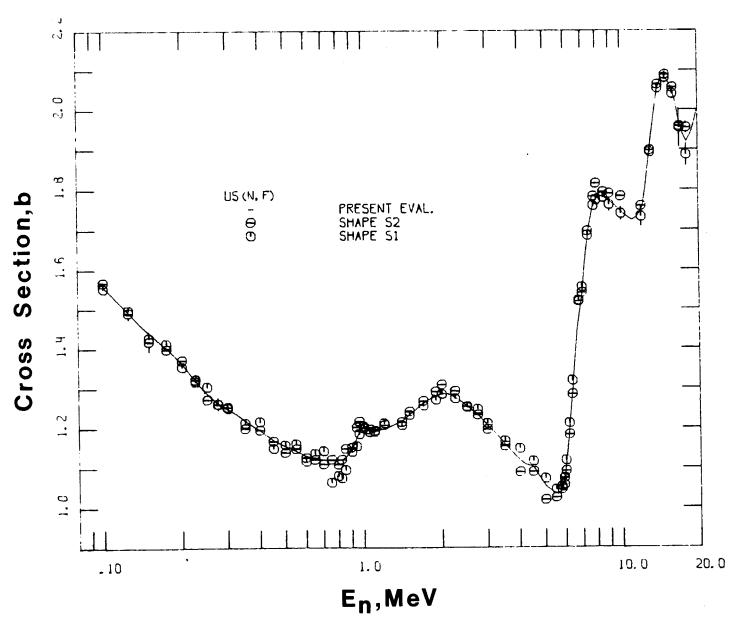


Fig 2. Comparison of the Shape of the Present Evaluation with the Actually Calculated Values. Shape S1 was obtained by starting at 20 MeV and S2 by starting at 0.1 MeV.

TABLE III. Normalization Factors

Set	Set Name	All Normal Factors	Selected Factors
1	Smith	1.006 ± 0.066	1.006 ± 0.066
2	Barton	$1.012 \pm 0.029$	$1.003 \pm 0.029$
71	Poenitz BND	$1.008 \pm 0.030$	$0.988 \pm 0.027$
74	Poenitz VSO4	$1.003 \pm 0.038$	$1.003 \pm 0.038$
73	Poenitz AA	$1.002 \pm 0.038$	$1.002 \pm 0.038$
4	Kari	$1.048 \pm 0.039$	$1.048 \pm 0.039$
16	Alkharov	$1.060 \pm 0.035$	_
12	Kuks	$1.051 \pm 0.041$	_
18	Cance	$1.007 \pm 0.038$	$1.007 \pm 0.038$
6	White	$1.032 \pm 0.042$	$1.032 \pm 0.042$
17	Wasson, Meier	$0.986 \pm 0.039$	$0.986 \pm 0.039$
52	Szabo	$1.012 \pm 0.032$	$1.012 \pm 0.032$
111	Kaeppeler	$1.054 \pm 0.037$	_
91	U. Midrigan	$1.019 \pm 0.024$	$1.019 \pm 0.024$
10	Wasson	$0.991 \pm 0.036$	$0.991 \pm 0.036$
251	Arct	$1.004 \pm 0.032$	$1.004 \pm 0.032$
14	Adamov	$1.048 \pm 0.021$	_
92	U. Michigan Cf	$1.006 \pm 0.021$	_
13	Heaton	1.001 ± 0.025	$1.001 \pm 0.025$
	ghted Average	1.018	1.007
	ted Average	1.019 ± 0.005	1.006 ± 0.004

TABLE IV. Average Differences of Data Sets from the Present

Set	Set Name	0.1 - 20.0 MeV	0.1 - 1.0 MeV	1.0 - 1.0 MeV
1	Smith	1.002 ± 0.058	_	1.002 ± 0.058
2	Barton	$1.010 \pm 0.021$	-	$1.010 \pm 0.021$
71	Poenitz BND	$0.989 \pm 0.020$	$0.998 \pm 0.019$	$0.984 \pm 0.021$
74	Poenitz VSO4	$0.996 \pm 0.037$	$0.996 \pm 0.037$	-
73	Poenitz AA	$0.997 \pm 0.037$	$0.997 \pm 0.037$	-
4	Kari	$1.040 \pm 0.029$	-	1.040 ± 0.029
16	Alkharov	$1.053 \pm 0.034^{a}$	-	$1.053 \pm 0.034^{6}$
12	Kuks	$1.045 \pm 0.038$	-	$1.045 \pm 0.038$
18	Cance	$1.000 \pm 0.023$	-	$1.000 \pm 0.023$
6	White	$1.032 \pm 0.034$	$1.017 \pm 0.042$	$1.039 \pm 0.027$
17	Wasson, Meier	$0.980 \pm 0.035$	$0.980 \pm 0.035$	$0.978 \pm 0.036$
52	Szabo	$1.005 \pm 0.027$	$1.018 \pm 0.027$	$0.998 \pm 0.028$
111	Kaeppeler	$1.046 \pm 0.033$	$1.053 \pm 0.032$	$1.037 \pm 0.033$
91	U. Midrigan	$1.013 \pm 0.021$	$1.013 \pm 0.021$	-
10	Wasson	$0.985 \pm 0.035$	$0.985 \pm 0.035$	-
251	Arlt	$0.998 \pm 0.011$	-	$0.998 \pm 0.011$
14	Adamov	$1.042 \pm 0.030^{a}$		
92	U. Midrigan	$1.000 \pm 0.014$	<del>-</del>	-
13	Heaton	$0.995 \pm 0.020$	-	-
Weigh	ted Average	$1.006 \pm 0.004$	$1.008 \pm 0.007$	$1.008 \pm 0.006$

<sup>&</sup>lt;sup>a</sup>Uncertainty doubled based upon the 2σ criteria.

sets from the present evaluations. The reason the weighted average is not 1.000 is due to the selection made in Table III but not made in Table IV and the accounting of the shape uncertainty in Table III and not in Table IV. The most important result shown in Table IV is that the choice of different energy ranges would not result in different normalizations. The change of the normalization due to inclusion of the  $^{252}\mathrm{Cf}$  fission spectrum averaged cross sections is only 0.2%.

### IV. EVALUATION RESULT AND COMPARISONS

Table V gives the result of the present evaluation of the  $^{235}\text{U}$  cross section which will be used in a later consistency fit with other data as input for 235U. Figure 3 compares the present result with the Evaluated Nuclear Data File ENDF/B IV. The present result is lower over most of the energy range and substantially so between 1.0 and 1.5 MeV and above 13 MeV. The difference above 13 MeV is the result of data inconcsistencies in older data and the improvement provided with more recent measurements not available for ENDF/B-IV but used in the present evaluation. The difference between 1.0 and 1.5 MeV is of importance in the interpretation of the average of the 235U cross section over a fission spectrum and for the interpretation of critical test facilities with a hard spectrum, as for example GODIVA. It appears that this difference is due to the selection of one experimental data set for ENDF/B-IV where many were available which predicted a different shape between 1 and 2 MeV. Figures 4-11 compare the present evaluation result with the absolute data used in the evaluation. Figures 12 and 13 compare the shape of the present evaluation with shape data which were normalized to the evaluated values. Figure 14 shows the data by Kari 39 and by White 14 normalized to the present result. This shows that these data agree rather well with the shape of the present evaluation but differ in normalization. Figures 15-17 show the energy range from 1 to 6 MeV in which a discrepancy exists between the data by Barton et al., 40, Kari, 39 Czirr and Sidhu<sup>38</sup> on the one hand and Szabo, 44 Poenitz, 41 and Carlson and Patrick46 on the other hand. The discrepancy is mainly in shape between 2 MeV and 6 MeV, except for the data by Kari which differ over the whole range in normalization and are between the two discrepant sets in shape. It is interesting to note that the measurements by Czirr and Sidhu $^{38}$  and by Carloson and Patrick $^{46}$  used the same basic experimental procedure but differ substantially in shape. Figure 18 compares the evaluation result with some older data sets not included in the present evaluation. Prominent data sets which had influenced evaluated nuclear data files up to ENDF/B-III (Allen and Furgeson, 47 Henkel, 48 and Diven 49) are 8% higher than the present evaluation result but appear to agree reasonably well in shape as can be seen in Fig. 19, where data from Fig. 18 were multiplied by a constant factor to better agree in magnitude with the present evaluation.

The average of the present evaluated  $^{235}$ U(n,f) cross section over the  $^{252}$ Cf spontaneous fission neutron spectrum is 1.215 b. This is to be compared with measurements by Heaton et al. $^{50}$  and by the University of Michigan. $^{51}$ The experimental values of (1.208  $\pm$  0.024) and (1.215  $\pm$  0.022) are in good agreement with the present result, however, a measurement reported by Abramov et al. $^{52}$  yielded (1.266  $\pm$  0.019)b, which suggests a substantially higher

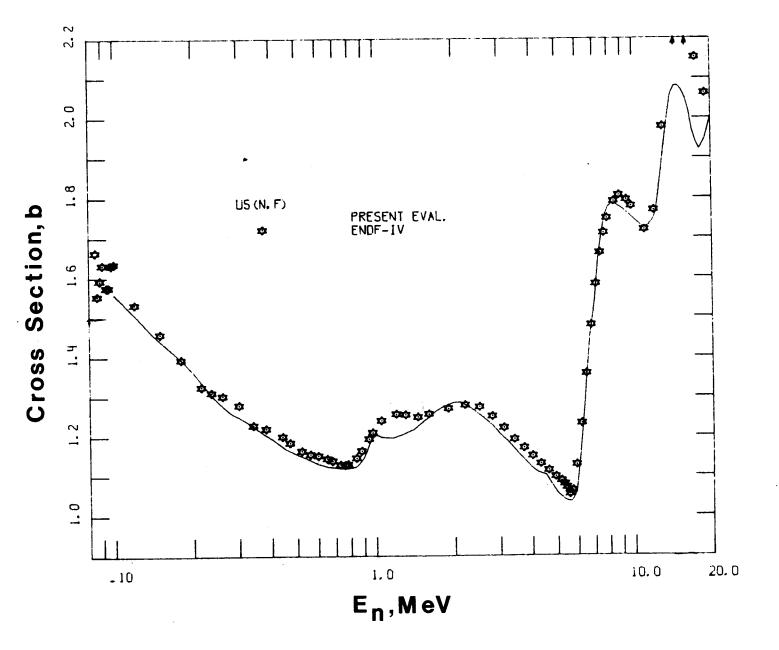


Fig. 3. Comparison of the Present Evaluated 235U(n,f) Cross Section with ENDF/B-IV.

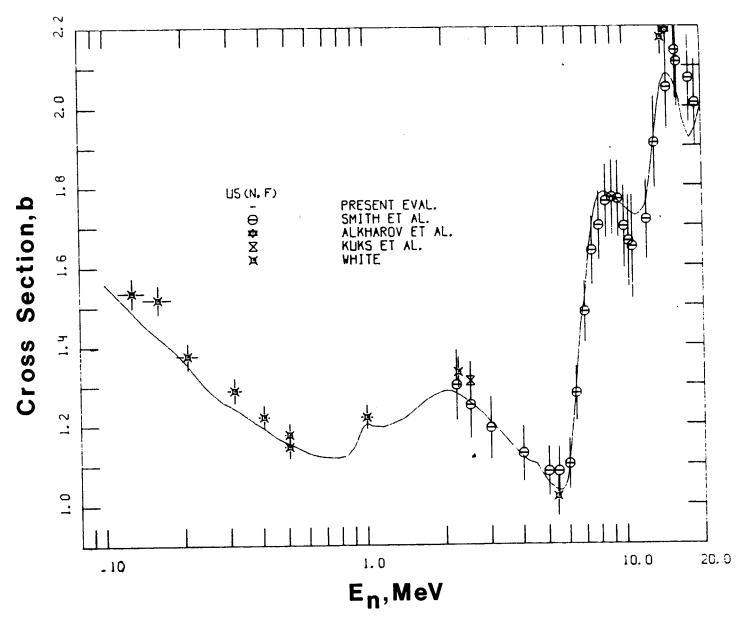


Fig. 4. Comparison of the Present Evaluated <sup>235</sup>U(n,f) Cross Section with Experimental Data.

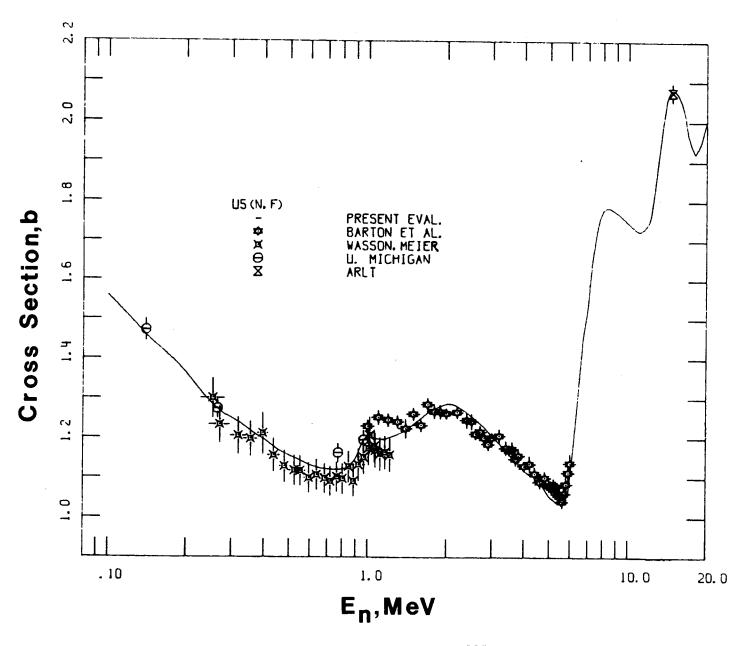


Fig. 5. Comparison of the Present Evaluated  $^{235}\text{U(n,f)}$  Cross Section with Experimental Data.

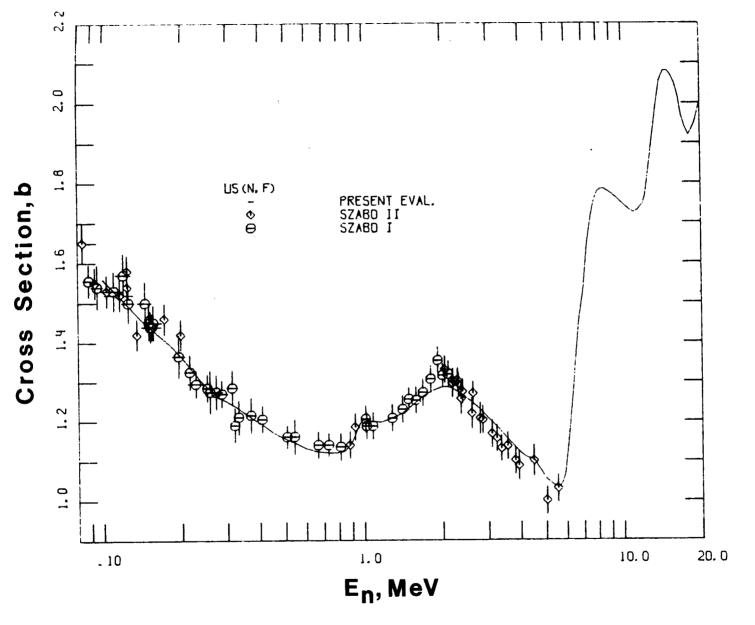


Fig. 6. Comparison of the Present Evaluated <sup>235</sup>U(n,f) Cross Section with Experimental Data.

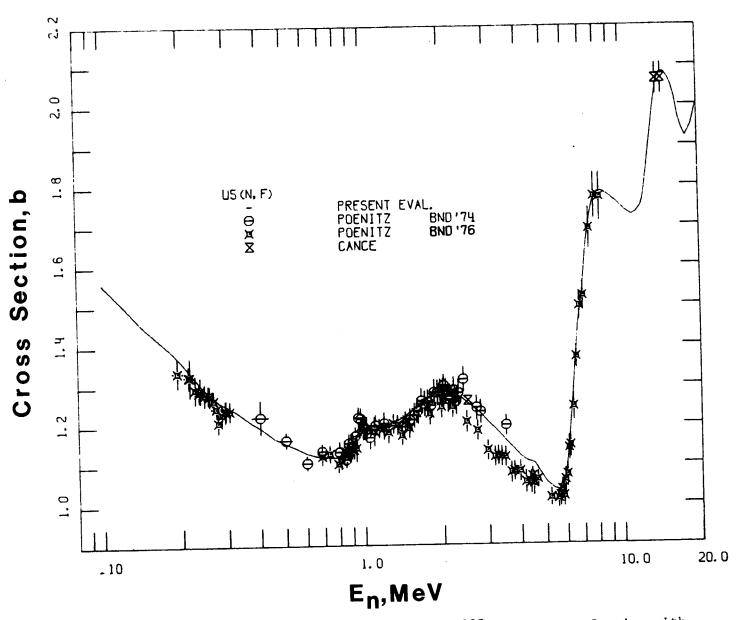


Fig. 7. Comparison of the Present Evaluated  $^{235}\text{U}(n,f)$  Cross Section with Experimental Data.

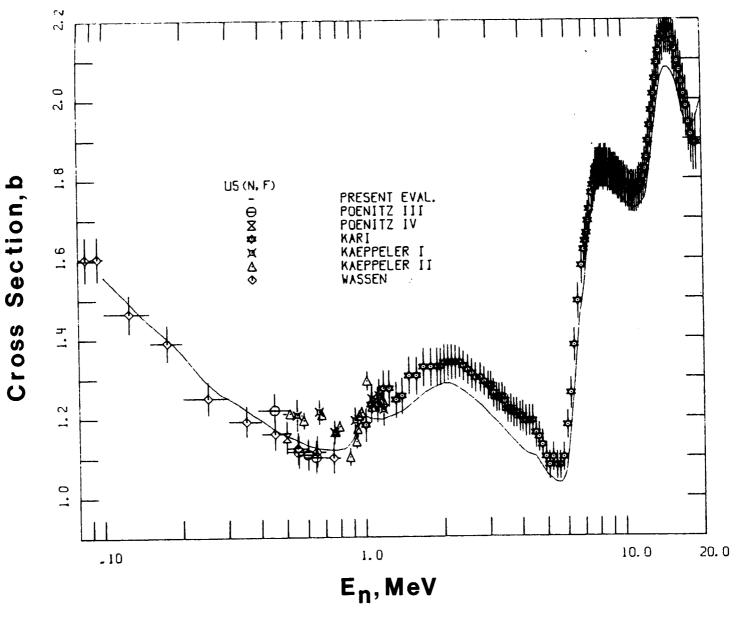


Fig. 8. Comparison of the Present Evaluated <sup>235</sup>U(n,f) Cross Section with Experimental Data.

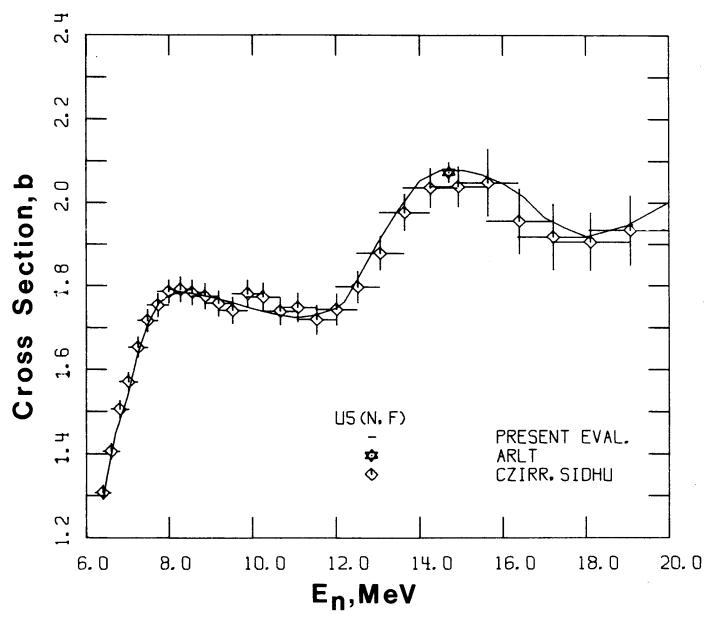


Fig. 9. Comparison of the Present Evaluated 235U(n,f) Cross Section with

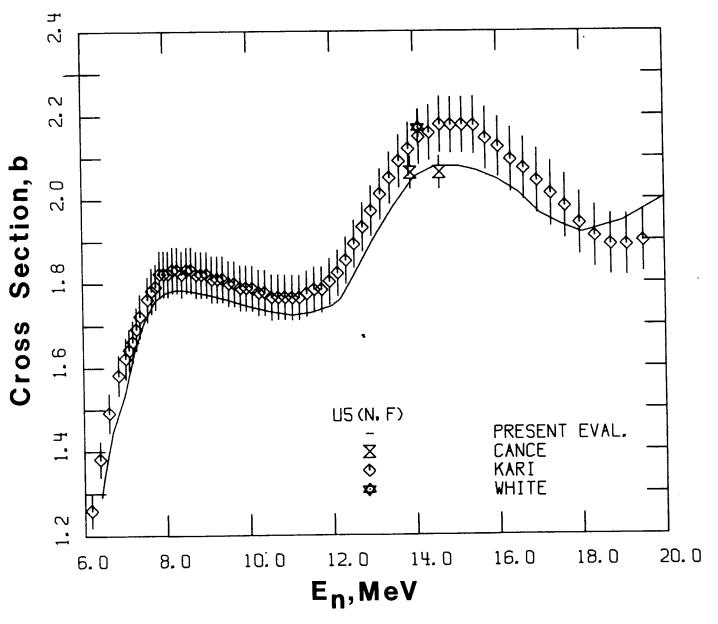


Fig. 10. Comparison of the Present Evaluated <sup>235</sup>U(n,f) Cross Section with Experimental Data.

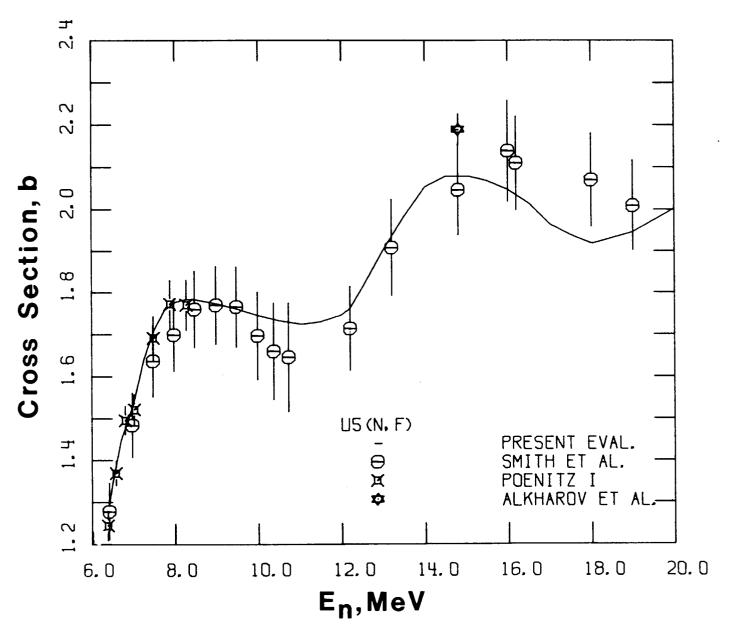


Fig. 11. Comparison of the Present Evaluated <sup>235</sup>U(n,f) Cross Section with Experimental Data.

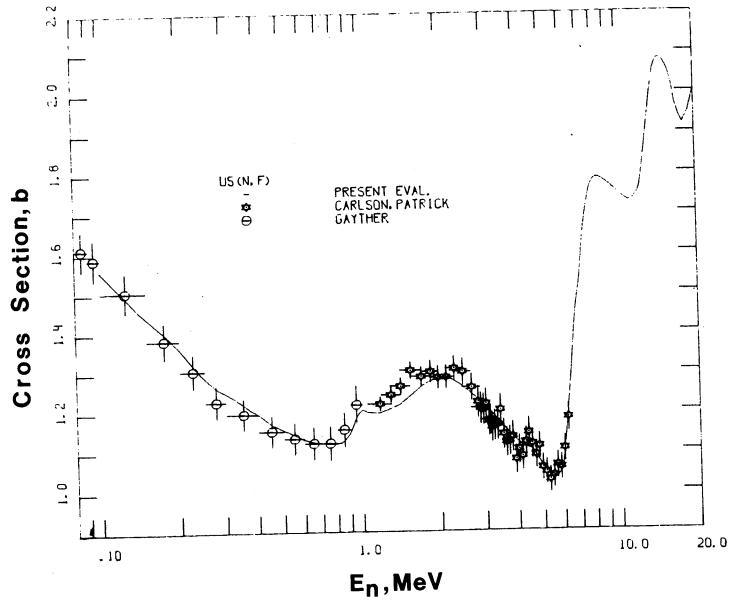


Fig. 12. Comparison of the Present Evaluated <sup>235</sup>U(n,f) Cross Section with Experimental Data.

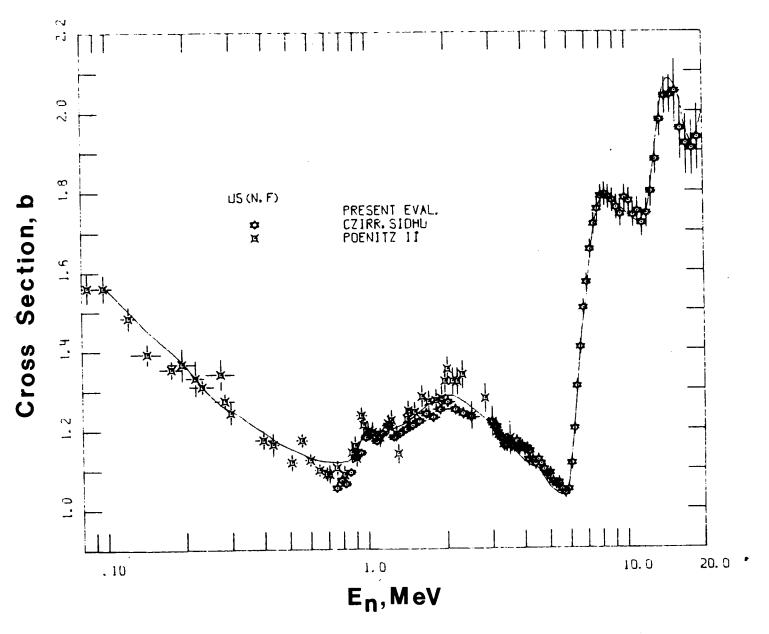


Fig. 13. Comparison of the Present Evaluated <sup>235</sup>U(n,f) Cross Section with Experimental Data.

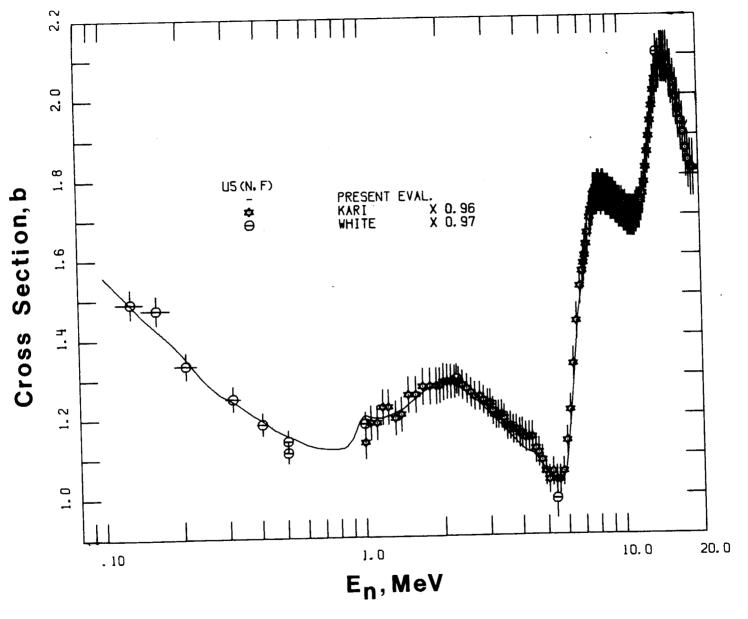


Fig. 14. Comparison of the Present Evaluated  $^{235}\text{U}(n,f)$  Cross Section with Experimental Data.

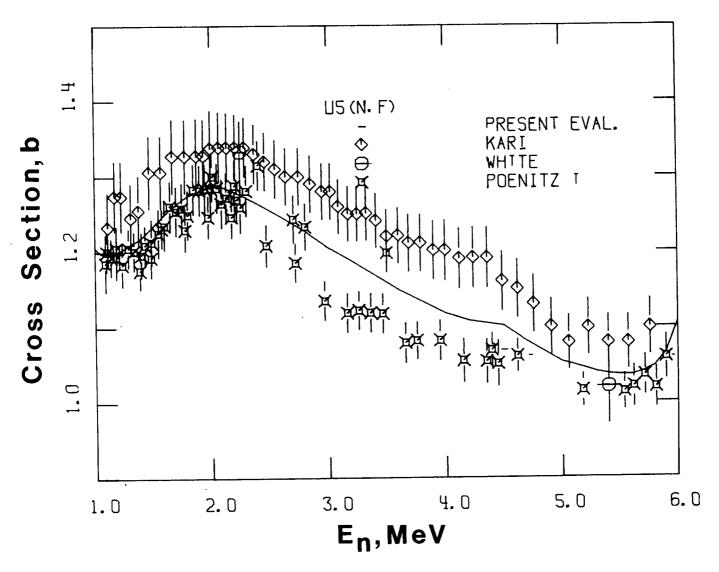


Fig. 15. Comparison of the Present Evaluated <sup>235</sup>U(n,f) Cross Section with Experimental Data.

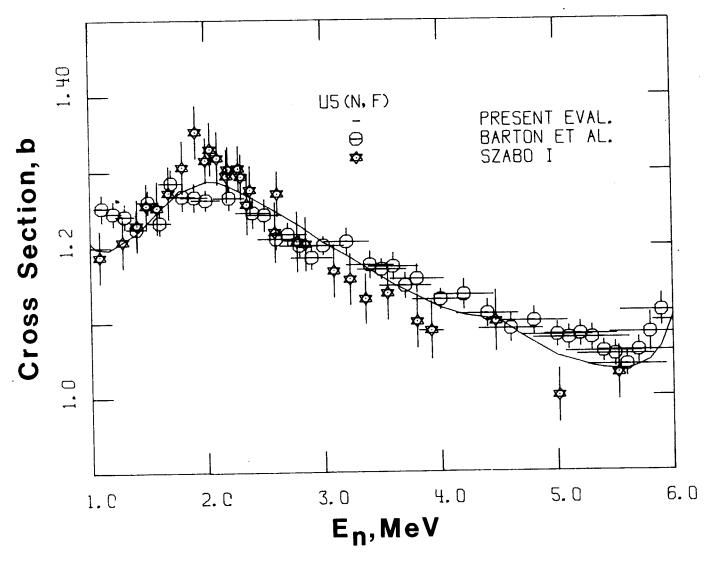


Fig. 16. Comparison of the Present Evaluated  $^{235}\text{U}(n,f)$  Cross Section with Experimental Data.

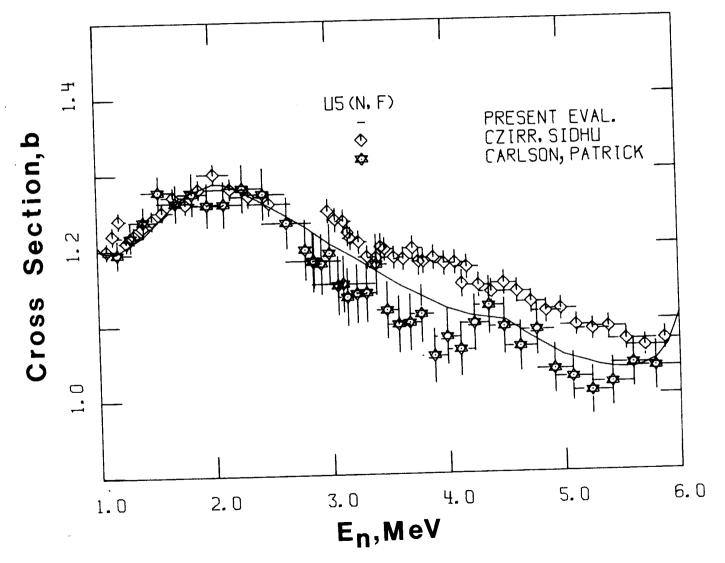


Fig. 17. Comparison of the Present Evaluated <sup>235</sup>U(n,f) Cross Section with Experimental Data.

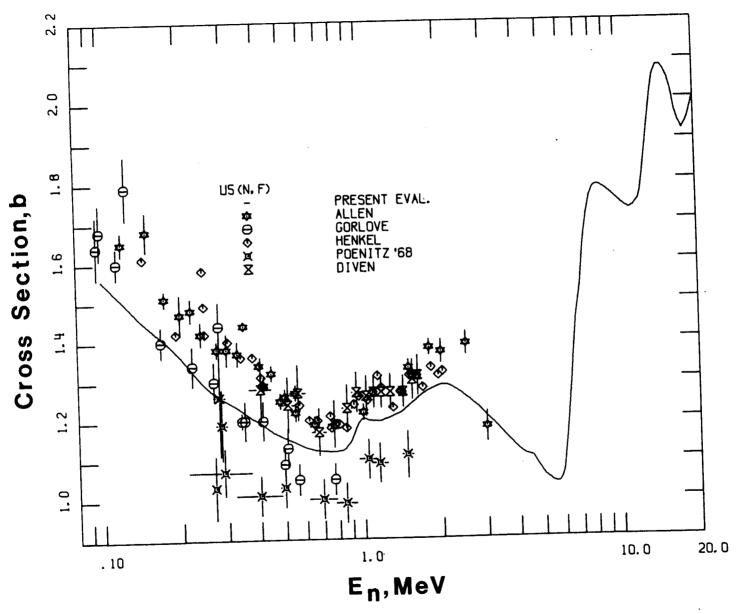


Fig. 18. Comparison of the Present Evaluated <sup>235</sup>U(n,f) Cross Section with Older Experimental Data Which were not Included in the Evaluation.

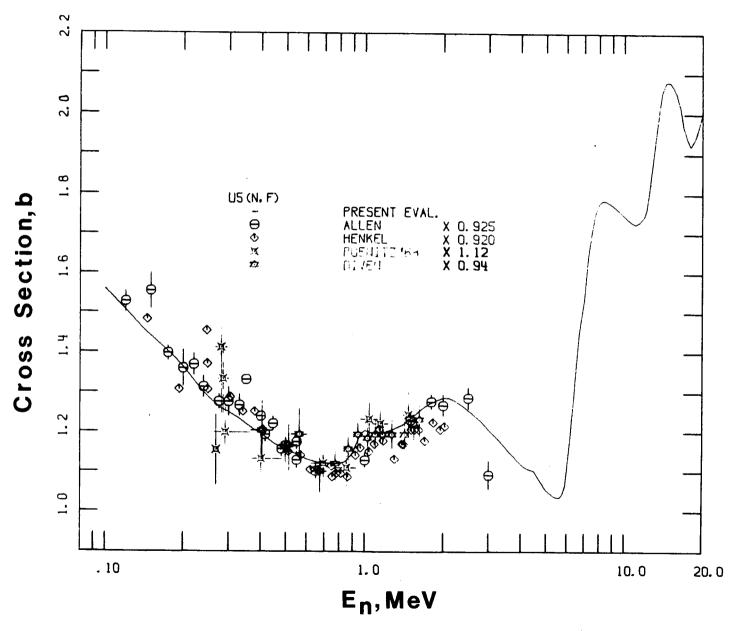


Fig. 19. Comparison of the Same Data as Shown in Fig. 18 but Normalized to the Present Result.

Table V. Results of the Present Evaluation

	Table V.	Results of the	Present E	valuation	
	E <sub>n</sub> , MeV	σ <b>,</b> b	E <sub>n</sub> , MeV	σ, b	
	0.100	1.556	3.200	1.186	
	0.100	1.503	3.600	1.148	
	0.140	1.457	4.000	1.117	
	0.140	1.439	4.200	1.107	
		1.423	4.500	1.100	
	0.160	1.392	4.700	1.079	
	0.180 0.200	1.361	5.000	1.052	
	0.220	1.327	5.200	1.043	
	0.240	1.298	5.300	1.038	
	0.250	1.286	5.400	1.035	
	0.260	1.276	5.500	1.034	
	0.280	1.258	5.600	1.034	
	0.300	1.248	5.700	1.039	
	0.325	1.235	5.800	1.046	
	0.350	1.219	5.900	1.065	
	0.375	1.205	6.000	1.105	
	0.400	1.194	6.200	1.196	
	0.425	1.181	6.400	1.290	
	0.450	1.169	6.500	1.348	
	0.475	1.160	6.700	1.447	
	0.500	1.154	7.000	1.534	
	0.540	1.144	7.250	1.639	
·	0.570	1.137	7.500	1.710	
	0.600	1.129	7.750	1.756	
	0.650	1.123	8.000	1.775 1.780	
	0.700	1.120	8.150		
	0.750	1.119	8.250	1.782 1.780	
	0.780	1.119	8.500	1.770	
	0.800	1.122	9 000	1.757	
	0.830	1.123	9.500	1.742	
	0.850	1.127	10.000	1.730	
	0.900	1.147	10.500	1.722	
	0.940	1.177	11.000	1.729	
	0.960	1.192	11.500	1.745	
	0.980	1.199	12.000	1.760	
	1.000	1.204	12.200	1.811	
	1.050	1.197	12.500	1.901	
	1.150	1.195	13.000	1.982	
	1.250	1.204	13.500	2.052	
	1.400	1.218	14.000	2.077	
	1.600	1.249	14.500	0 077	
	1.700	1.263	15.000	- 0/5	
	1.800	1.274	15.500	- 011	
	1.900	1.280	16.000	- 010	
	2.000	1.286	16.650	1 0/2	
	2.100	1.285	17.000		
	2.400	1.263	17.500		
	2.600	1.245	18.000		
	2.800	1.226	19.000 20.000	- 222	
	3.000		20.000	<b>,</b> —	

 $235\,\mathrm{U}(\mathrm{n,f})$  cross section. The values masured by NBS<sup>50</sup> and the University of Michigan are considered very significant because a neutron source calibrated in an international source mesurement intercomparison was used in both experiments.

The average over the <sup>252</sup>Cf spontaneous fission neutron spectrum can be considered an integral over the differential cross section. However, the experiments used to measure the average cross section are very similar in design to the differential cross section experiments and the results were used here in the evaluation of the normalization of the differential cross section. The next logical step to test the evaluated <sup>235</sup>U(n,f) cross section would be calculations of the parameters of the benchmark critical reactor test facilities. However, such calculations are sensitive to uncertainties of other data. The only benchmark facility considered here is GODIVA which consists essentially of <sup>235</sup>U and thus depends on fewer other data than other critical benchmarks.

The results of recent calculations of  $k_{\rm eff}$  and reaction ratios for GODIVA with ENDF/B-V data indicate that the calculated spectrum is too hard. This was concluded from the reaction ratios  $\langle 2^8 \text{C}/2^8 \text{f} \rangle$  which was underpredicted by  $\sim 12\%$  and  $\langle 2^8 \text{f}/2^5 \text{f} \rangle$  which was overpredicted by  $\sim 6\%$ . The differential data for the latter ratio are very well known. Therefore,  $\langle 2^8 \text{f}/2^5 \text{f} \rangle$  was used to adjust the spectrum of GODIVA by changing the inelastic scattering of  $\langle 2^{35} \text{U} \rangle$  by  $\sim 15\%$ .  $k_{\rm eff}$  and the reaction ratios were then calculated using sensitivity coefficients. The results are for the presently evaluated  $\langle 2^{35} \text{U}(\text{n,f}) \rangle$  cross section:

k <sub>eff</sub>	0.999
<28f/25 <sub>f</sub> >	1.003
<28c/25f>	0.983

# V. CONCLUSIONS AND RECOMMENDATIONS

The result of the evaluation of the <sup>235</sup>U(n,f) cross section by an objective evaluation technique is very well supported by the experimental data which were reported with the lowest uncertainties (Arlt et al., <sup>35</sup> Barton et al., <sup>40</sup> Knoll, <sup>51</sup> Cance and Grenier, and Heaton et al., <sup>50</sup>) and is in good agreement with many other data sets (Szabo, <sup>44</sup> Poenitz, <sup>42</sup> Smith et al.). Agreement with data by Wasson is reasonable after renormalization of these data with an evaluated resonance integral between 7.8 eV and 11.0 eV of 243.7 beV. Some of the more recently reported data are somewhat lower than the evaluation results (Poenitz, <sup>41</sup> Wasson and Meier <sup>45</sup>) and some are higher (Adamov et al., <sup>52</sup> Kari<sup>39</sup>).

The shape of the cross section is very well established below 700 keV. The step in the cross section between 800 keV and 1 MeV is about 8%, however, the exact nature of this step is not well known. Several experiments, unfortunately, exclude the range of this step or do not cover a wide enough range. This results in some uncertainty of the above 8% which is considered a very important value.

"It is recommended to measure the shape with good statistics and resolution as well as high point density between  $\sim\!600$  keV and 1.4 MeV."

The plateau in the cross section shape between 1.0 - 1.5 MeV is well established, however, the rise between 1.5 and 2.0 MeV is somewhat uncertain. Data by Szabo<sup>44</sup> and Grey Neutron Detector data by Poenitz<sup>42</sup> show a larger increase than the Black Neutron Detector data by Poenitz<sup>44</sup> and recent measurements relative to the H(n,n) cross section by Czirr and Sidhu, Kari<sup>39</sup> and Carlson and Patrick.<sup>46</sup> The data by Barton et al.<sup>40</sup> show a very flat shape in this range. It is believed that the shape is well-enough established by the majority of the data in this range.

There is a shape discrepancy between the plateau range (1 - 1.5 MeV) and the dip at ~5-6 MeV. there are two groups of data, the higher group 38,39,40 appears to predict a convex shape and the lower group 41,42,44,46 predicts a concave shape. The data by Barton et al. seem to "step-up" around 3 MeV, and the data by Carlson and Patrick show a peak at ~4.5 MeV. The dip appears to be at lower energy and much wider in the data by Kari, Carlson and Patrick, Szabo, and Poenitz than in the data by Barton et al. and Czirr and Sidhu.

"Measurements of the shape between the plateau at  $1.0 - 1.5 \, \text{MeV}$  and  $6 \, \text{MeV}$  are recommended to resolve the shape discrepancy in this range."

The shape between 6 MeV and 14 MeV is reasonably well established, but large uncertainties exist above 14 MeV.

The normalization of the  $^{235}\text{U}$  cross section appears to be well established by a large number of experiments. The latest reported data seem to increase the dispersion. However, the uncertainties of these data are such that they cannot suggest values differing from the present evaluation result one way or another.

"It is recommended that future measurements be made with an uncertainty of  $\sim 1\%$  in order to be significant."

#### APPENDIX I. The Data File

#### Smith, Henkel, Nobles (Set 1)

The present data source is a listing distributed by L. Stewart at a CSEWG meeting at Brookhaven National Laboratory in September 12, 1978. According to this distribution the cross sections were recalculated in 1975 by G. Hansen using values found in old data books. This listing replaces a previous reanalysis from 1968 in which the major changes from the original values were due to multiple scattering corrections. The new data listing quotes only statistical uncertainties which differ in some points by more than a factor 3 from the statistical uncertainties quoted in the 1968 distribution. The total uncertainty was recalculated from the 1968 quoted total uncertainties replacing the statistical uncertainty with the present (1975) quoted value(s) by

SQRT(E\*\*2 - D\*\*2), where E,D,S refer to quantities given in the 1968 listing.

Reference: R. K. Smith et al., <u>Bull. Am. Phys. Soc.</u>, <u>2</u>, 196 (K4), 5704. See Figs. 4 and 11.

```
U5 (N.F) SET
               1/128
                            SMITH ET AL.
DA TA
 ,2220E 01 .0000E 00 ,0000E 00 ,1301E 01 .8980E-01 ,2732E-01
.2500E 01 .0000E 00 .0000E 00 .1250E 01 .8350E-01 .7500E-02
.3000E 01 .0000E 00 .0000E 00 .1192E 01 .7830E-01 .7152E-02
.4000E 01 .0000E 00 .0000E 00 .1128E 01 .6960E-01
                                                     . 1466 E= 01
.50 00 E 01 ,00 00 E 00 .00 00 E 00 .10 83 E 01 ,62 50 E-01 .16 24 E-01
.5460E 01 .0000E 00 .0000E 00 .1083E 01 .6250E-01
                                                     .7581E-02
.6000E 01 .0000E 00
                     .0000E 00
                               .1101E 01 .6390E-01
                                                    . 99 09 E= 02
.6410E 01 .0000E 00 .0000E 00 .1278E 01 .6840E-01
                                                    .1406E-01
.6970E 01 .0000E 00 .0000E 00 .1484E 01 .7790E-01
                                                     .1484E-01
.7470E 01 .0000E 00
                     .0000E 00 .1637E 01 .8580E-01 .1473E-01
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                                                    .1359E-01
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                                                     .1413E-01
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                                                    . 15 27 E- 01
.1037E 02 .0000E 00 .0000E 00
                               .1660E 01
                                          .1151E 00
                                                    . 14 94 E= 01
.10/3E 02 .0000E 00 .0000E 00
                               .1646E 01 .1300E 00 .2140E-01
.1220E 02 .0000E 00
                    .0000E 00
                               .1714E 01
                                          .1005E 00
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,1320E 02 ,0000E 00 ,0000E 00
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                               .2069E 01 .1109E 00
                                                     .2690E-01
.1900E 02 .0000E 00
                    .0000E 00
                               .2008E 01 .1077E 00
                                                     .2610E-01
.1/00E 22 .0000E 00 .0000E 00 .2154E 01 .1138E 00 .2800E-01
```

# Barton et al. (Set 2)

The data source is the NSE publication. Energy scale errors have been suggested for these measurements, and it was pointed out that such energy error would cause substantial cross section changes due to the energy dependence of the reference H(n,n) cross section. The energy errors as suggested appear unlikely and the question was debated at the 1976 ANL meeting. Any change of the data seems unjustified. The energy uncertainty was not given in the paper and only a limit for the resolution  $\geq 6\%$  was reported in the paper, therefore a resolution of 6% was assumed at all energies. The energy uncertainty was assumed to be 20% of the resolution (see Section III.2).

This data set is the one with the least quoted uncertainty ( $\sim$ 1.5%), however, the uncertainty of the reference cross section due to energy uncertainties adds considerably to this value.

Reference: D. M. Barton et al., Nucl. Sci. Eng., 60, 369, 1976.

See Figs. 5 and 16.

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                        .7800E-01
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                                              .1688E-01
                                                          .9929E-02
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                       . 84 00 E- 01
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                                 .1081E 01 .1682E-01 .1190E-01
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### Barton et al. (Set 2) (Continued)

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.5100E 01 .0000E 00 .3060E 00 .1077E 01 .1615E-01 .9685E-02
.5200E 01 .0000E 00 .3120E 00 .1082E 01 .1690E-01 .1082E-01
.5300E 01
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                    .3180E 00
.5400E 01
          .0000E 00
                    .3240E 00 .1059E 01 .1471E-01 .7409E-02
.5500E 01
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                    .3300E 00
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.5700E 01
                               .1060E 01 .1726E-01 .1167E-01
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                    .3420E 00
.5800E 01
         .0000E 00
                    .3480E 00
                               .1084E 01 .2622E-01 .2277E-01
.5900E 01 .0000E 00 .3540E 00
                               .1113E 01 .2138E-01 .1669E-01
.60 00 E 01 .00 00 E 00 .36 00 E 00 .11 37 E 01 .24 60 E-01 .20 47 E-01
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### Czirr and Sidhu (Set 31)

Two sets of measurements of the shape were made overlapping at 3.5 MeV. The low energy set has a gap due to experimental problems which partly extended also to the remaining points of this set around 3.5 MeV.

The statistical uncertainty of the overlap range of the two sets was added as a systematic uncertainty to the high energy set (0.9%).

The data by Czirr and Sidhu are quoted with a very low uncertainty and thus strongly influence the shape. This results in the only major problem of the shape evaluation where a discrepancy in the shape below 1 MeV is created (see Fig. 2). Breaking up the data set in the overlap range (~3.5 MeV) does not change the evaluated shape significantly. The data source was the Tables in the NSE publications.

Reference: J. B. Czirr and G. S. Sidhu, <u>Nucl. Sci. Eng.</u>, <u>60</u>, 383, 1976. See Figs. 9, 16 and 17.

```
SZIRR SIDHU 1+11
  05 (N.F.) SET 33/128
DATA
./540E 00 .5030E-33 .3100F-01 .1080E 01 .1200E-01 .1080E-31
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           .0001E 00 .3750E-01 .1120E 01 .1100E-01 .8960E-02
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                     .4000E-01 .1160E 01 .1100E-01 .9280E-02
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 .9/9UE 00
 .1026E 01 .740JE-05 .4900E-01 .1220E 01 .1200E-01 .9760E-02
           .00000 0) .53006-01 .1200E 01 .1100E-01 .9600E-02
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           .0000 - 00 .0700E-01 .1220E 01 .1200E-01 .9760E-02
 .1132E 01
 .1191E 01 .000JE 00 .6100E-01 .1240E 01 .1100E-01 .9920E-02
 .1254E 01 .0000E 00 .6600E-01 .1210E 01 .1100E-01 .9680E-02
 .1323E 01 .0000E 30 .7200E-01 .1220E 01 .1100E-01 .9760E-02
 .139HE 01 .0003E 00 .7800E-01 .1230E 01 .1100E-01 .9840E-02
                                .1240E 01 .1300E-01 .9920E-02
 .14/9E 01 .0000 BD 00E-01
 .1568E 01 .0000E 00 .9300E-01
                                .1250E 01 .1100E-01 .1250E-71
 .1667E 01 .0000E 30 .1015E 00 .1270E 01 .1300E-01 .1016E-01
                                .1260E 01 .1200E-01 .1134E-01
 .1/71E 01 .000JE 00 .1110E 00
 . 15 0/E 01 . 00 30 € 00 . 12 20 € 00 . 12 80 € 01 . 13 00 €-01 . 11 52 €-01
 .2015E 01 .2000E-02 .1350E 00
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                                .1280E 31 .1400E-01 .1289E-31
 . 215/E 01 .0000E 00 .1500E 00
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 .2315E 01 .0000E 05 .1565E 00
 .2490E 01 .00JUE UN .1855E 00
                                .1260E u1 .1600c=01 .1386E=01
 .2990E 01 .00 00E 00 .6300E-01 .1249E 01 .1573E-01 .1124E-01
 .3050E 01 ,4000E-02 .6500E-01 .1237E 31 .1565E-01 .1113E-01
 .31 20 E 01 .00 00 E 90 .65 00 E 01 .12 35 E 01 .15 64 E 01 .11 11 E 01
 .3,56E 01 .0039E on .0300E 08 .1220E 01 .1800E-01 .1464E-01
 .0180E 01 .000JE 90 .6500F=01 .1212E 01 .1549E=01 .1091E=01
 .3250E 01 .0000E 00 .7000E-01 .1207E 01 .1546E-01 .1086E-01
 . 3320E 01 .0000E 90 .7500E-01 .1187E 01 .1533E-01 .1068E-01
 .34 UUE 01 .00 00 E Ju .75 00 E-01 .11 66 E 81 .15 33 E-01 .10 67 E-01
 .3438E 01 .0003E JD .0000F 00 .1200E J1 .1500E-01 .1680E-01
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### Czirr and Sidhu (Set 31) (Continued)

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# Czirr and Sidhu (Set 31) (Continued)

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.1640E 02 .00 CDE 00 .79 COE 00 .20 U1E 01 .81 03 E-01 .76 04 E-01 .17 22 E 02 .00 U3E 00 .85 50 E 00 .19 62 E U1 .31 93 E-01 .76 52 E-01 .18 11 E U2 .00 00 E U0 .92 50 E 00 .19 50 E U1 .72 17 E-01 .66 30 E-01 .19 07 E 02 .00 00 E U0 .79 50 E U0 .19 70 E U1 .86 84 E-01 .81 10 E-01 .20 10 E U2 .67 GJE-01 .10 79 E U1 .20 48 E U1 .13 13 E 00 .12 70 E 00
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## Kari (Set 4)

The data were reported in a KFK report and presented at the Harwell Conference on Neutron Physics and Applications. It is here assumed that these data are replacing previous shape data reported by Leugers et al. at the ANL Specialists Meeting on Fission Cross Sections in 1976. The data reported by Kari are absolute. However, a notable fact is that the fission counting efficiency in this experiment was only 75%. This data set differs substantially above 13 MeV from the previously reported data by Leugers et al.

Reference: K. Kari, Nuclear Research Center Karlsruhe Report, KFK 2673, 1978.

See Figs. 8, 10, 14 and 15.

```
KARI(LEUGERS 78)
                 4/128
  US (N.F) SET
DATA
                        .0000E 00 .1162E 01 .4344E-01 .1424E-01
 .1000E 01 .0000E 00
                                   .1233E 01 .4530E-01 .1485E-01
 .1050E 01 .0000E
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#### Kari (Set 4) (Continued)

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#### Szabo et al.

The present data source is the listing of final values in Szabo's paper presented at the Specialists' Meeting on Fission - Cross Sections in 1976 at ANL. The measurements reported at 1970 ANL were made with the fission chamber of White, therefore, this set is only used as shape data because their normalization is not independent from White's values. This also applied for one subset of data presented at the Conference on Neutron Physics - 1973 in Kiev and the new data presented at Argonne in 1976. All other data were made with independent fission chambers. An obvious bias between the results using White's chamber and the other chambers cannot be seen.

Reference: I. Szabo and J. P. Marquette, NEANDC/NEACRP Specialists' Meeting on Fast Neutron Fission Cross Sections, Argonne National Laboratory, ANL-76-90, 208 (1976).

See Figs. 6 and 16.

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#### Szabo et al. (Continued)

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# Szabo et al. (Continued)

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### White (Set 6)

Present data source is the publication in J. Nucl. Energy. ENDF/B-V values for H(n,n) were substituted for all energies below 5 MeV. This caused changes of a few tenths of one percent for most values but 1 percent at one energy. The 5.4 MeV value is based on a recalculation by G. Hansen (memorandum by L. Stewart, August 24, 1978) of a correction factor of 1.0199 for useing ENDF/B-V cross section data for the H(n,n) reference and a relativistic correction.

A case could be made to renormalize these data upward by approximately 1% based on the  $T_{1/2}$  measurement of U-234 by White and the presently known value of ~2.447  $\cdot$  10<sup>4</sup> y; however, the relationship of the foils used in the  $T_{1/2}$  - determination and the cross sections measurements is not exactly known. Szabo confirms that the mass derived with the high  $T_{1/2}$  - value is within 1% of White's values.

Reference: P. H. White, J. Nucl. Energy A/B, 19, 325, 1965.

See Figs. 4, 10, 14 and 15.

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U5 (N.F) SET 6/128
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 .1410E 02 .0000E 00 .5000E-01 .2170E 01 .4340E-01 .0000E 00
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# Poenitz, BND (Set 71)

Measurements with a Black Neutron Detector (BND) were reported in 1974 and the measurements were extended to higher and lower energies in 1977. The measurements in 1974 were shape measurements with two absolute values at 800 keV and at 3.5 MeV. All values reported in 1977 were absolute. The measurement at 3.5 MeV was made with a sample provided by EURATOM, the measurements at 800 keV and those reported in 1977 were made with different samples provided by Meadows. The latter data set has been revised for more recent determinations of the mass scale of the samples involved (1.3%). The 800 keV value was measured with another sample by Meadows and is unchanged.

# Poenitz, GND (Set 72)

This is a set of data measured with a Grey Neutron Detector (GND), which was reported in 1974. These are only shape data.

# Poenitz, AA (Set 73)

This set contains absolute values obtained with the associated activity technique. Values were reported in 1974.

# Poenitz, VSO4

This set contains an absolute value measured with a  $VSO_4$  - Bath.

References: W. P. Poenitz, Nucl. Sci. Eng., 53, 370, 1974, Nucl. Sci. Eng., 60, 894, 1977.

See Figs. 7, 8, 11, 13 and 15.

US(N.F) SET 71 PENITZ I DATA

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. 15 78 E
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. 21 78 E
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                              , 80 00 E- 02
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. 37 56 E
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. 39 55 E
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. 41 53 E
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. 4351 E
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. 44 49 E
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                              .1070E 00
. 51 79 E
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                              . 44 00 E- 01
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                                                             . 23 69 E- 01
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                              . 72 00 E- 01
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. 58 09 E
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               . 16 00 E- 01
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                              . 69 00 E- 01
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                              . 62 00 E= 01
                                             . 13 69 E
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. 65 79 E
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. 68 D3 E
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                                             . 15 21 E
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. 70 25 E
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                              . 48 00 E- 01
                                             . 16 91 E
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. 74 78 E
          01
              .00 00 E
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                                             . 17 72 E
. 75 75 E
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                                                            .6119E-01
                                                                            . 32 27 E= U1
.8275E 01
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U5(N.F) SET 72
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DA TA
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                                                           n1 .76 00 E-01
 . 35 00 E- 01
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 . 14 25 E
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 . 12 78 E
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 . 16 05 E
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 . 22 04 E
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                                 , 67 00 E- 01
 . 23 04 E
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.24 99 E 01 .00 00 E 00 .64 00 E 01 .12 50 E 01 .36 00 E 01 .28 20 E 01 .00 00 E 00 .45 33 E 01 .12 94 E 01 .38 00 E 01 .30 00 E 01 .00 00 E 00 .58 00 E 01 .12 34 E 01 .40 00 E 01 .35 00 E 01 .00 00 E 00 .53 00 E 01 .11 92 E 01 .45 00 E 01
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U5(N.F) SET 73 PØENITZ III

DATA

.4480 E 00 .00 00 E 00 .60 00 E 01 .12 20 E 01 .44 00 E 01

.55 25 E 00 .00 00 E 00 .55 00 E 01 .11 15 E 01 .42 00 E 01

.60 10 E 00 .00 00 E 00 .55 50 E 01 .11 08 E 01 .40 50 E 01

.64 40 E 00 .00 00 E 00 .65 00 E 01 .11 01 E 01 .42 00 E 01
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## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76

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U5(N,F) SET 74 P DE NITZ IV
DA TA
. 49 80 E+ 00 . 00 00 E+ 00 . 00 00 E+ 00 . 11 51 E+ 01 . 42 00 E= 01
** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76
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#### Wasson (Set 10)

Data were reported at the 1976 ANL meeting normalized to a 7.8-11 eV integral reported by Deruytter. Normalization to the average of several measurements as given in Table I and reference to the thermal cross section of ENDF/B-V causes an upward normalization by 2.2%. The uncertainty of the normalized data consists of several components which were not added by the author. The various uncertainties were summarized by Poenitz.<sup>5</sup> The uncertainty for the 7.8-11 eV integral was substituted with the present value of Table I. This yields a value of 2.5% for the uncertainties of the normalization which is added to a typical 1.6-2.0% uncertainty of the quoted data. The data in the keV energy range were measured relative to the H(n,n) cross section and an analysis by Gammel was used for this cross section. The data were normalized here with the ENDF/B-V H(n,n) cross section.

Reference: 0. A. Wasson, NEANDC/NEACRP Specialists' Meeting on the Fast Neutron Cross Sections, Argonne National Laboratory, ANL-76-90, 183, 1976.

See Figs. 1 and 8.

```
UD (N.F.) SET 10/128
                            WASSEN
UATA
 ,5>00E-02 .0000E 00 .5000E-03 .4055E 01 .3082E-02 .4022E-01
 .obu0E-02 .0000E 00 .5000E-03 .3345E u1 .1318E n0 .4021E-01
           .0000E 00 .5000E-03 .3305E 01 .1281E 00 .4021E-01
 •/500E-02
                                 .3010E U1 .1160E 00
.0500E-02
           .00 u3E y0 .5000E-03
                                                      .4020E-01
. 95 00 E- 02 . 00 00 E 00 . 50 00 E- 03 . 32 13 E 01 . 12 11 E 00 . 40 20 E- 01
                                 .2532E 01
                                           .8802E-01
.1500E-01
           .0000E 00 .5000E-02
                                                      .1004E-01
.2500E-01 .0000E 00 .5000E-02 .2157E u1 .7488E-01 .2006E-01
                                .1981E U1 .7433E-01
.3500E=01
           .0000E 00 .5000E-02
                                                      .2005E-01
           .00 00 E 00 .50 00 E-02 .1816 E 01 .6270 E-01
. 45 00 E- 01
                                                      .2003E=01.
.5500E-01 .6000E 00 .5000E-02 .1766E 01 .6173E-01 .2002E-01
           .0000E 00 .5000E-02
                                 .1730E 01 .5979E=01
.6500E-01
                                                      .2001F-01
./500E-01 .0600E 06 .5000E-02
                                .1644E u1 .5706E-01 .2000E-01
                     •50 00 E= 02
•ช500E=01
           .000002 00
                                .1602E 01 .5730E-01
                                                      .1999E-01
. 95 00 E- 01
           . Oblige E. ad
                      02 € £ 00 نار •
                                .1604E 01 .5733E-01 .1998E-01
.1250E 00
           .00 u0E d0
                      .2500E-01
                                .1465E 01 .4972E-01 .9984E-02
                      .2500E-01
                                 .1391E 01 .4723E-01
                                                      . 99 77 E- UZ
.1750E 00
           .0000E 00
           .0000E 00 .5000E-01 .1251E 01 .4224E-01 .9974E-02
.2500E 00
                                 .1192E 01 .4019E-01 .9976E-02
                      .5000E-01
.3500E 00
           . OO JUE OU
           .0000E 00 .5000E-01 .1161E 01 .4197E-01 .9982E-02
.4500E 00
                                .1123E 01 .4099E-01 .9989E-02
.5500E 00
           .0000E 00 .5000E=01
           .006JE 00 .5000E-01 .1115E 01 .4028E-01 .9997E-02
.65 UOE 00
.7500E 00 .0000E 00 .5000E+01 .1100E 01 .3993E+01 .1000E+01
```

# Kaeppeler (Sets 111 and 112)

Measurements were made relative to H(n,n). The data were revised to use ENDF/B-V for the reference cross section. Only the set 111 is absolute data.

Reference: F. Kaeppeler, Nuclear Research Center Karlsruhe report, KFK 1772, 1973.

```
U5(N,F) SET111
                                                                                     K AE PP EL ER I
 DA TA
     .5460E 00 .0000E 00 .2200E-01 .1205E 01 .4104E-01
     .6620E 00 .000E 00 .2300E-01 .1213E 01 .3159E-01
     .7580 E 00 ,0000 E 00 .2300 E-01 .1163 E 01 .3026 E-01
     .9080E 00 .0000E 00 .2200E=01 .1193E 01
                                                                                                                                                                                    . 34 60 E= 01
     .1057E 01 .0000E 00 .2600E-01 .1249E 01 .3744E-01
     .1125E 01 .0000E 00 .2500E-01 .1258E 01 .4270E-01
    .1175E 01 .0000E 00 .2500E-01 .1223E 01 .4151E-01
                          *# 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 ## 76 
   U5(N,F) SET 112
                                                                                   KAPPPELER TI
DATA
   .5130E 00 .0000E 00 .3200E-01 .1208E 01 .1089E-01
   .5000E 00 .0000E 00 .2000E-01 .1191E 01 .2147E-01
   .6780E 00 .0000E 00 .2100E-01 .1206E 01 .1450E-01
   .7670E 00
                                             .0000E 00
                                                                                          .2000E-01
                                                                                                                                       .1164E 01 .1048E-01
   .7950E 00 .0000E 00 .2000E-01 .1177E 01 .1414E-01
   .8720E 00 .0000E 00
                                                                                           .2000E-01
                                                                                                                                        .1102E 01 .2314E-01
  .9200E 00
                                                                                          .2200E-01 .1141E 01 .1711E-01
                                              .000CE 00
  .9300E 00
                                                                                           .2000E-01 .1172E 01 .2227E-01
                                              .0000E 00
  . 9450E 00
                                              .0000E 00
                                                                                          . 24 00 E= 01
                                                                                                                                      .1206E 01 .1327E-01
  .9660E 00
                                              .0000E 00
                                                                                           .2100E-01 .1213E J1 .1456E-01
  . 1013E 01
                                             .0000E 00
                                                                                          .2000E-01 .1294E 01 .2457E-01
  .1060E 01 .0000E 00 .2200E-01 .1226E G1 .1472E-01
  .1164E 01 .0000E 00 .4000E-01 .1245E 01 .2239E-01
                       ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 ** 76 *
```

### U. Michigan (Set 91)

Values for several photoneutron sources were reported at various occasions. The current values are used in the evaluation.

Data are from a private communication with G. Knoll and represent values to be published in Annals of Nucl. Sci., September 1978).

```
US (N.F.) SET 91/128 U. MICHIGAN I

DATA
.14 DOE 00 .00 00 00 00 .00 000 00 .14716 UL .29 00 E= 01 .00 00 E 66
.26 DOE 00 .00 00 00 .00 00 .12748 01 .26 00 E= 01 .00 00 8 60
.77 OOE 00 .00 00 00 .00 00 00 .11628 01 .25 00 E= 01 .00 00 8 00
.96 40 E 00 .00 00 E 00 .00 00 .11958 01 .26 00 E= 01 .00 00 E 00
```

## U. Michigan II (Set 92)

An average value over the Cf spectrum was obtained with the same  $MnSO_4$  bath and foils used in the measurements with the photoneutron sources.

Reference: G. F. Knoll, Proc. Symp. on Neutron Standards and Applications, NBS Special Publication 493, 3041, 1977.

See Fig. 5.

# Carlson and Patrick (Set 151)

The shape of the cross section was measured relative to the H(n,n) cross section. The measurements were reported at the Harwell Conference on Neutron Physics and Applications and the data are still preliminary. Measurements were made up to 20 MeV but data only up to 6 MeV were provided for the present evaluation. The data consists of two sets which overlap around 3 MeV. Combining the two data sets requires the addition of 2.2% for the statistical uncertainty of the overlap range to the uncertainty of either data set. The 2.2% were here added to the uncertainty of the data above 3 MeV.

Reference: A. D. Carlson and B. H. Patrick, Conference on Neutron Physics and Applications, Harwell, England (1978).

See Figs. 12 and 17.

```
UD (N.F) SET153/128
                                  CARLSON . PATRICK
 DATA
  •1171E U1
              . 22 d1 K- U1
                          .1250 E 00 .1195 E 01 .1872 E-01 .17 00 E-01
  •12 d8E 01
             • 26 31 E= 01
                           • 1085E
                                       .1217E 01 .1941E-01
                                   00
                                                                • 17 00 E- 01
  . 1464E U1
              . 29 94 E- 01
                           • 1230 E
                                   00
                                       .1236E U1
                                                    . 2055 E- 01
                                                                . 1900 E-01
  ・1535E 01
              .3423E-01
                          +1405E
                                   ŨÜ
                                       .1277E 01
                                                   .2185E-01
                                                                .2000F-01
  .1586E 01
              .3941E-01
                          .1625E
                                   00
                                       .1262E
                                                U1
                                                    .2439E-01
                                                                .2200E-01
 . 1536F
          01
              . 4456E-UI
                          • 1220E
                                   ΟÛ
                                       .1274E
                                                01
                                                   · 2828E-01
                                                                .2600E=01
 • 1956E
              .4932E-01
          01
                          •1350€
                                   00
                                       .1259E UI
                                                   .2910E-01
                                                                .2800E-01
 • 21 UÚ E
          01
              . 54 78 E- 01
                          . 15 UDE
                                   Ú0
                                       .1260E
                                               01
                                                   . 30 34 E- 01
                                                                . 29 00 E- 01
 ・ととりを
          U1
             . 61 11 E- 01
                          . 1675E
                                  0.0
                                       .1281E
                                               U1
                                                   .3201E-01
                                                                .3100E-01
 . 24 JEE 01
              . 66 44 E= 01
                          • 1675E
                                       . 1273E
                                   00
                                               01
                                                   . 34 21 E- 01
                                                                . 33 00 E= 01
 .2635E 01
             .7699E-01
                          • 2115E
                                   00
                                       .1234E 01
                                                   .3387E=01
                                                                .3300E-01
 .2768E 01
             • 60 00 E 00
                          • 0000E
                                   00
                                      .1198E
                                                   .3969E-01
                                               01
                                                                .2800E-01
 ・さかりラモ
         01
             .0000E 00
                          . UU 00 E
                                   00
                                       .1182E 01
                                                   .3945E-01
                                                                .2800E-01
 . 2 3 6 U E
         01
             •6795E=01
                          .2380E
                                   0.0
                                       .1103E
                                               U1
                                                   .3531E-01
                                                                .3400E-01
 . CY 24 E
         U1
             . Buddle no
                          •0000E
                                  ÜÜ
                                      ,1179E
                                               01
                                                   .394UE-01
                                                               .2700E-01
 • 2795E
         01
             • NOUNE GO
                          ,0000E 00
                                      .1193E
                                               u1
                                                  .3889E-01
                                                               .2700E-01
 . 3169E
         01
             .6000E 00
                          .0000E 00
                                      .1150E
                                               U1
                                                   .3822E-01
                                                               .2700E-01
 • 3114E
         Ü1
             •9891E=01
                          .2720E 00
                                      .1152E
                                               J1
                                                   .3662E=01
                                                               .3600E-01
 . 31 4/E
         U1
             . 16 05 E- 01
                          . 78 68 E- 01
                                      . 11 35 E
                                               Ü1
                                                   . 38 00 E- 01
                                                               . 27 00 E- 01
 . 3227E U1
             • 10 44 E= 01
                         . 61 72 E-01
                                      .1139E
                                               01
                                                   .3838E-01
                                                               . 28 00 E- 01
 .3311E 01
             .1034E-01
                         .8491E-01
                                      . 11 40 E
                                               01
                                                  .3552E-01
                                                               .2800E-01
 . 3397E ú1
             .1127E-01
                         • 0526F-01
                                      .1177E
                                               V1
                                                  .3983E=01
                                                               .2900E-01
 .348/E 01
             .11726-U1
                         .9180E-01
                                      .1117E
                                               01
                                                  .3772E-01
                                                               .2700E-01
3581 E
             . 12 20 E- 01
         ü1
                         ・ y5 53 E= U1
                                      .1095E
                                               01
                                                  . 37 17 E- 01
                                                               . 27 00 E= 01
, 36 /OE U1
             .1270E-01
                         . 9446F-U1
                                      .1100E
                                                  .3725E-01
                                               01
                                                               .2700E-01
. 3/80E 61
             . 1323E- 61
                         • 15 36 E €0
                                     .1111E
                                              U1 .3768€-01
                                                               . 27 00 E- 01
. 30 85 E 01
            . 13 /yb= u1
                         • 10 80 H
                                  ÜÜ
                                     . 10 35 E
                                              J1
                                                 . 35 88 E = 01
                                                               . 26 00 E= 01
•3796E 01
            · 14 33 E= (:1
                         • 11 26 F
                                  60
                                     • 10 au E
                                              IJ1
                                                 . 36 49 E- 01
                                                              • 27 00 E= 01
.4111E 01
            .1500E-01
                         •1176E
                                 00
                                     .1063E
                                              31
                                                 .3589E-01
• 42 31 E U1
                                                              .2600E-01
            · 15 55 E= 61
                         • 1228 E
                                 Ûυ
                                     .1090E
                                              01
                                                 .3724=-01
                                                              . 27 00 E-01
· 4356E 01
            .1637E=01
                         ·1283E 00
                                     . 11 21 E
                                                  . 36 11 b= 01
                                              J1
                                                              . 28 00 E- 11
.4437E 01
            .1711E-61
                         .1341E 00
                                     .1093E
                                             u1
                                                  .3712E-01
                                                              .2700E-01
. 40 25 E 01
            . 1790 E- 01
                        .1403E Cu
                                     . 10 66 E
                                              01
                                                  . 33 44 E- 01
                                                              . 23 00 E- U1
•4/68E 01
           · 18 74 E = 01
                        .1469 E 00
                                     .1080E 01
                                                 .3396E-01
                                                             . 23 00 E-01
. 1718E 01
           .1963E-01 .1540E 00
                                     .1035E 01 .3260E-01 .2200E-01
```

## Carlson and Patrick (Set 151) (Continued)

```
.5076E 01 .2059E-01 .1515E 00 .1024E 01 .3221F-01 .2200E-01 .5241E 01 .2160E-01 .1694E 00 .1005E 01 .3169E-01 .2200E-01 .5415E 01 .2268E-01 .1779E 00 .1016E 01 .3207F-01 .2200E-01 .5597E 01 .2384E-01 .1870E 00 .1041E 01 .3287E-01 .2200E-01 .5789E 01 .2507E-01 .1968E 00 .1036E 01 .3280E-01 .2200E-01 .5991E 01 .2639E-01 .2072E 00 .1082E 01 .3385E-01 .2300E-01 .6203E 01 .2781E-01 .2183E 00 .1158E 01 .3591E-01 .2400E-01
```

# Cancé and Grenier (Set 18)

An absolute value at 14,6 MeV was obtained with the associated particle technique and reported at the NEANDC/NEACRP - Specialists Meeting on Fast Neutron Fission Cross Sections. Additional values at 13.9 MeV and at 2.5 MeV were reported at the Conference on Neutron Physics and Applications at Harwell. The neutron flux was compared at 2.5 MeV with the directional counter by Szabo and at 14 MeV with a Black Neutron Detector.

Reference: M. Cancé and G. Grenier, Nucl. Sci. and Eng., 68, 197 (1978).

See Figs. 7 and 10.

UP (N,F) SET 18/128 CANCE DATA

- .2>00E 01 .00000E 00 .0000E 00 .1261E 01 .0000E 00 .0000E 00 .1390E 02 .0000E 00 .0000E 00 .2062E 01 .3900E-01 .0000E 00
- .1460E 02 .0000E 00 .0000E 00 .2063E 01 .3900E-01 .0000E 00

## Wasson and Meier (Set 17)

Absolute cross section data were obtained with a Black Neutron Detector. The mass of the  $^{235}\text{U}$  in the fission chamber is based upon a comparison with a standard NBS foil set and is therefore not independent from the measurement by Heaton et al., (Set 13). The data are preliminary and some additional values were measured recently but are not included in the present evaluation.

Reference: Private communication by A. O. Wasson, National Bureau of Standards, 1978.

See Fig. 5.

```
05 (N.F.) SET 17/128
                             WASSIN, MEIER
DATA
 .2540E 00 .5000E-02 .2750E-01 .1300E 01 .5100E-01 .2080E-01
 .2700E 00 .5000E-02 .2500E-01 .1233E 01 .4800E-01 .1849E-01
 .3180E 00 .5000E-02 .2150E-01 .1205E 01 .4800E-01 .1807E-01
           .5000E-02 .2200E-01
                                 .1197E 01 .4500E-01 .1676E-01
 .3550E 00
                                 .1211E 01 .5400E-01 .1574E-01
 .3950E 00
           .5000E-02 .1900E-01
 .4350E 00
           .5000E-02 .2350E-01
                                 .1156E 01 .4300E-01 .1387E-01
 .4780E 00
                                 .1128E 01 ,4100E-01 ,1241E-01
           ,50 CO E = 02 , 19 00 E = 01
 .5230E 00
           .50 00 E- 02 .2450 E- 01
                                 .11 18E 01 .39 00 E = 01 .78 26 E = 02
           .50 UUE-U2 .2450E-U1
                                 .1117E U1 .390UE-01 .8936E-02
 .5520E 00
           .50 00 E- 02 . 25 00 E- 01
 .5950E 00
                                 .1099E ul .3900t-01 .9891E-02
 .6370E 00
           .5000E-02 .2600E-01 .1107E 01 .3900E-01 .1107E-01
                                .1098E
                                        01 .3900 E-01 .1098 E-01
 .6840E 00
           .50 00 E- U2 .2350 E- U1
           .60 00 E-02 .27 00 E-01
 .7190E 00
                                . 1U 91 E
                                        01 .3300E-01 .7637E-02
 .7630E 00
           .6000E=02 .2600E=01
                                .1102E u1 .3900E-01 .1102E-01
                                 .1097E
                                        01 .3900 E-01 .1097 E-01
 . 5010E 00
           .6000E-02 .3100E-01
 .8450E 00
           .6000E-02 .2950E-01
                                 .1127E 01 .4000E-01 .1127E-61
 .8830E 00
           .6000E-02 .2950E-01
                                 .1091E
                                        01 .4000E-01 .1091E-01
                                        01 .41 00 E= 01 .11 32 E= 01
 .9220E 00
           .5000E-02 .5700E-01
                                 . 11 32 E
 .963UE 00
           , 10 00 E- 61 . 43 50 E- 01
                                .1151E 01 .4300E-01 .1381E-01
           .50 UNE-02 .2250E-01
                                 .1174E 61 .4400E-01 .1057E-01
 .1010E 01
 .1021E 01 .5000E-02 .2100E-01 .1207E
                                        U1 .4700 E-01 .1328 E-01
 .1065E 01 .5000E-02 .2250E-01
                                .1179E U1 .4300E-01 .1179E-U1
 .1071E 01
           .5000E-02 .1900E-01
                                 .1168E U1 .4400E-01 .1285E-01
 •1119E 01 •5000E-02 •2050E-01 •1159E 01 •4300E-01 •1159E-01
 .1167E 01 .5000E-02 .2200E-01 .1163E 01 .4300E-01 .1163E-01
 .1217E 01 .5000E-62 .2250E-01 .1157E 01 .4300E-01 .1157E-01
```

## Gayther (Set 8)

The shape of the cross section was measured with a Grey Neutron Detector. The fission events were measured by detecting the fast fission neutrons, thus the actual measured quantity was  $\nu$  .  $\sigma_f$ .

Reference: D. B. Gayther, <u>Proc. of Conference on Nuclear Cross Sections and Technology</u>, NBS Sp. Publ. 425, Vol. II, 564 (1975).

### See Fig. 12.

```
UD (N.F) SET
                 3/120
                               GAYTHER
            .00 00 E Ju .50 00 E+03 .78 81 E D1 .3231 E 00 .00 00 E On
 .10 UU E- 02
 ,2500E-02 ,0000E NO .5000E-03 .5722E U1 .2232E 00 .0000E 00
           .00000E 00 .5000E-03 .5045E 01 .1867E 00 .0000E 00
 . 35 00 E- 02
 . 45 00 E+ 02 . 30 00 E 00 . 50 00 E- 03 . 4474 € 01 . 1566 € 00 . 00 00 E
            .0000E 00
 ,つつ 00 E - 02
                       . Di. 00E=03
                                   .4046E 01 .1336E 00 .0000E
 .65 00 E- 02 .00 GO € GO
                       • 50 00 E= 03 . 33 79 E
                                           61 .1081E 00 .0000E
 . /5 UUE-02
            .0000E 00
                       .5000E=03
                                   .3280E 01 .1017E 00 .0000E
 • 35 UU E= 02
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. 95 UU Ē 00 , 80 00 € 00 , 50 00 € 01 , 12 18 € 01 , 48 72 E - 01 , 00 00 € 00
```

# Kuks et al. (Set 12)

A value was obtained at 2.5 MeV using the associated particle technique.

Reference: I. M. Kuks et al., Conf. on Neutron Physics, Kiev, Vol. 4, 18, (1973).

See Fig. 4.

U5(N,F) SET 12/128 KUKS ET AL.

DATA

.2500E 01 .0000E 00 .0000E 00 .1310E 01 .5000E-01 .0000E 00

# Alkharov et al. (Set 16)

A value was obtained at 14.8 MeV with the associated particle technique.

Reference: See V. M. Adamov et al., Proc. of a Symposium Neutron Standards and Applications, NBS Spec. Publ. 493, 313, (1977).

UD(N.F) SET 16/126 ALKHAREV ET AL.

DATA

.148UE 02 .0000E 00 .0000E 00 .2188E 01 .3700E-01 .0000E 00

## Arlt (Set 251)

An absolute value was measured at  $14.7\ \mathrm{MeV}$  using the associated particle technique.

Reference: R. Arlt et al., International Nuclear Data Committee report

INDC/GDR/-7.16, 10, 1978.

See Figs.: 5 and 9

U5 (N.F) SET251/128 ARLT DRESDEN
DATA:
.1470E 02 .0000E 00 .0000E 00 .2073E 01 .2360E-01 .0000E 00

## Adamov et al. (Set 14)

An average of the cross section over the  $^{252}\mathrm{Cf}$  fission neutron spectrum was measured. The technique was based upon a coincidence technique.

Reference: V. M. Adamov et al., <u>Proceedings of a Symposium on Neutron Standards</u> and Applications, NBS Spec. Publ. 493, 313, (1977).

U5(N,F) SET 14 ADAMOV ,2100E 01 .0000E 00 .0000E 00 .1265E 01 .1900E-01

\*\* 76 \*\* 76 \*\* 76 \*\* 76 \*\* 76 \*\* 76 \*\* 76 \*\* 76 \*\* 76 \*\* 76 \*\* 76 \*\* 76 \*\* 76 \*\* 76

APPENDIX II: The Evaluation of <sup>235</sup>U(n,f) above 100 KeV for ENDF/B-V

The  $^{235}$ U(n,f) cross section of ENDF/B-V above 100 KeV was derived from a preliminary version of the present evaluation. Small differences in the shape are due to the later discovery that two data  $sets^{28},^{39}$  used the analysis of the H(n,n) cross section by  $Gammel^{29}$  instead of  $ENDF/B-V^{16},^{17}$  values. However, the major difference is in normalization. The members of the Subcommittee on Normalizations and Standards of the Cross Section Evaluation Working Group (CSEWG) selected normalization factors closely corresponding to the first column of Table III, but the value by Arlt et al.  $^{35}$  was excluded because it was not well documented at that time. Also not used in the normalization of ENDF/B-V were the averages over the  $^{252}Cf$  - spontaneous fission neutron spectrum. ENDF/B-V is  $\sim 1.3\%$  higher in normalization than the present evaluated result with which it is compared in Fig. 20. ENDF/B-V values are given in Table. VI.

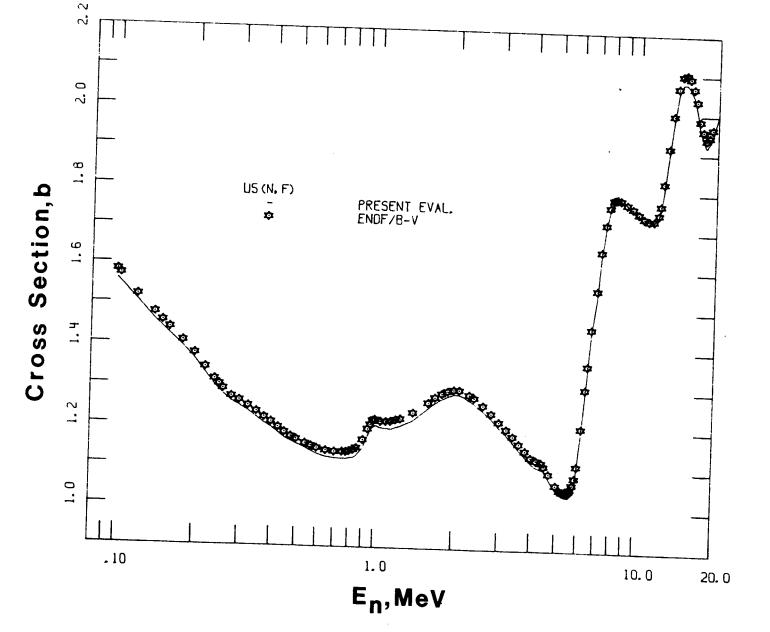


Fig. 20. Comparison of the Present Evaluated  $^{235}U(n,f)$  Cross Section with FNDF/R-V

Table VI. 235U(n,f) of ENDF/B-V

 E <sub>n</sub> , MeV	σ, b	E <sub>n</sub> , MeV	σ, b		
 0.100	1.581	3.400 3.600	1.184		
0.103	1.572 1.520	3.600 3.800	1.165 1.148		
0.120 0.140	1.476	4.000	1.132		
0.150	1.457 1.440	4.200 4.400	1.125 1.120		
0.160 0.180	1.408	4.500	1.111		
0.200	1.377	4.700	1.092 1.064		
0.220 0.240	1.343 1.314	5.000 5.200	1.052		
0.250	1.302	5.300 5.400	1.048 1.047		
0.260 0.280	1.291 1.272	5.500	1.047		
0.300	1.262	5.600	1.049 1.051		
0.325 0.350	1.249 1.235	5.640 5.700	1.055		
0.375	1.221	5.800	1.066		
0.400	1.209	5.900 6.000	1.083 1.112		
0.425 0.450	1.196 1.184	6.200	1.207		
0.475	1.174	6.400 6.500	1.306 1.364		
0.500 0.540	1.167 1.157	6.700	1.456		
0.570	1.151	7.000	1.553		
0.600	1.145 1.140	7.250 7.500	1.650 1.719		
0.650 0.700	1.137	7.750	1.763		
0.750	1.137	8.000 8.150	1.782 1.784		
0.780	1.137 1.139	8.250	1.784		
0.800 0.830	1.142	8.500	1.782 1.772		
0.850	1.147	9.000 9.500	1.762		
0.900 0.940	1.168 1.195	10.000	1.749		
0 <b>.9</b> 60	1.207	10.500 11.000	1.738 1.732		
0.980 1.000	1.217 1.220	11.500	1.732		
1.050	1.215	12.000	1.748		
1.100	1.215	12.200 12.500	1.771 1.826		
1.150 1.200	1.216 1.220	13.000	1.915		
1.250	1.223	13.500	1.998		
1.400	1.239	14.000	2.068 2.099	_	
1.600	1.264	14.500 15.000	2.103	•	
1.700	1.278 1.288	15.500	2.093		
1.800 1.900	1.294	16.000	2.068		
2.000	1.298	16.500	2.036		
2.100	1.297	17.000	1.986		
2.300	1.286	17.500	1.960 1.939		
2.400	1.278	18.000 18.500	1.939		
2.600	1.259 1.240	19.000	1.966		
2.800 3.000	1.219	19.500	1.990		
3.200	1.201	20.000	2.024		

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